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APPARATUS USED IN DETERMINING COEFFICIENTS OF FRICTION

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The reports of research published in this magazine are necessarily qualified by the conditions of the tests from which the data are obtained. Whenever it is deemed possible to do so, generalizations are drawn from the results of the tests; and, unless this is done, the conclusions formulated must be considered as specifically pertinent only to described conditions.

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DETERMINATION OF COEFFICIENTS OF FRICTION OF SLIDING BEARINGS FOR BRIDGES

BY THE DIVISION OF TESTS, BUREAU OF PUBLIC ROADS

Reported by GEORGE W. DAVIS, Associate Engineer of Tests

XPANSION and contraction in bridge superstruc-E tures are generally provided for by means of bearings at one end which permit the structure to move longitudinally with respect to its supports. For the smaller structures, these bearings are frequently of the sliding type in which a metal sole plate, rigidly connected to the superstructure, slides on a metal bearing which is rigidly connected to the substructure. The efficiency of these sliding bearings in preventing temperature stresses in the superstructure and overturning forces in the supporting substructure is inversely proportional to the frictional forces developed between the moving parts of the bridge.

As early as 1922 the Bureau of Public Roads, realizing the paucity of reliable test data as to the magnitude of these frictional forces, considered making an investigation. Some preliminary work was done in 1925 and in 1929 a more comprehensive series of tests was inaugurated. This program of tests, after several interruptions, has finally been completed and is made the sub-

ject of this report.

The coefficient of friction for sliding bearing plates was determined under varying pressures comparable to those usually employed in bridge design. Lateral pressure to cause slip was applied slowly and uniformly and the amount of movement at each slip was such as to approximate closely that caused by temperature changes in the field.

In making these tests several variables were con-

sidered, namely:

1. Materials.

2. Bearing pressures. 3. Surface finishes.

Direction of movement in relation to the direction in which the plates were finished.

5. The effect of lubrication.

The effect of rust.

The effect of electrolytic action on unlike materials in contact in the presence of salt water or salt air.

EFFECTS OF SEVERAL VARIABLES STUDIED IN INVESTIGATION

A more detailed discussion of the consideration given these variables follows.

1. Materials.—Fourteen different materials were used in these tests.

Bronzes:

Bronze A, A. S. T. M. Specification B22-21, class A. Bronze B, A. S. T. M. Specification B22-21, class B. Bronze C, A. S. T. M. Specification B22-21, class C. Bronze D, A. S. T. M. Specification B22-21, class D. Phosphor bronze E, A. S. T. M. Specification B22-21, class A.1

Phosphor bronze F, A.S.T.M. Specification B22-21, Class B.1

Lead bronze 22 (approximately 22 percent lead).

Lead bronze 17 (approximately 17 percent lead).

structural steel. Stainless steel.

Malleable, A. S. T. M. Specification A47–30. Cast, A. S. T. M. Specification A48–29, heavy cast-

The physical and chemical properties of these materials are shown in table 1.

2. Bearing pressures.—Tests were made under unit bearing pressures of 250, 500, 750, and 1,000 pounds per square inch.

3. Surface finishes.—Six surface finishes were used on the test specimens.

Planed finishes:

- Pc-A coarse-planed finish produced by using a round-nosed tool with a radius of 1/16 inch, at a rate of 45 cutting strokes per minute, with a lateral feed of 0.018 inch per stroke, and taking a cut of 1/4 inch. This produced a somewhat coarse, striated finish.
- P_M—A medium-planed finish produced with the same tool at the same rate and taking the same cut as above but using a lateral feed of 0.009 inch per stroke. This produced a medium smooth finish.
- P_F—A smooth or fine-planed finish produced with a flat-nosed tool % inch wide, used at a rate of 45 strokes per minute, with a lateral feed of ¼ inch per stroke, and taking a cut of 0.002 inch.

Rolled or planished finish:

R-Plates were finished as under PF with a flatnosed tool and then rolled with a hardened steel roller ¾ inch wide and 2½ inches in diameter rigidly bolted to the head of the planer. The feed of this roller was ¼ inch per stroke and the rate 26 strokes per minute. The roller, with its face set 0.005 inch below the surface of the specimen, was fed in 1/4-inch increments once transversely across the specimen. During this passage of the roller across the test plate all portions of the surface were rolled twice longitudinally, once on the forward stroke and once on the reverse stroke of the planer head. The roller was then depressed an additional 0.005 inch and

Lead bronze 8 (approximately 8 percent lead). Cast steel, A.S.T.M. Specification A27-24, class B, medium grade. Rolled steel, A.S.T.M. Specification A7-29,

¹ These materials as furnished were cold rolled and were classed by the manufacturer as phosphor bronze. They actually contained less phosphorus than bronzes A, B, C, and D.

TABLE 1.—Chemical composition and physical characteristics of materials tested CHEMICAL COMPOSITION I

					Bronzes						Steel		Iro	on
	A. S. T.	M. Spec	ification	B22-21	Phos		Le	ad bronz	08	Cast, A. S. T. M. A27-24.	Rolled,	Stainless	Malleable,	Cast,
	A	В	С	D	Е	F	22 per- cent	17 per- cent	8 per- cent	class B, medium	A7-29, structural	Statniess	A47-30	A48-29, heavy
Copper, percent	79. 45 19. 87	81. 95 17. 17	80. 17 10, 66	87. 43 10. 30	89. 20 10. 55	94. 30 5. 16	70.38 5.36	75. 70 4. 96	82.00 9.06			**********		
Lead, percentZinc, percent	0.05	0. 10 0. 20	8. 47	0. 32 1. 65			22. 33 1. 68	16, 90 2, 21	8. 37 0. 24	********				
Phosphorus, percentAll others, percent	0.40	0. 18 0. 35 0. 05	0. 15 0. 55	0. 15 0. 15	0.09	0.14	0, 14	0.14	0, 21	0.42	0.011	0.028		********
Carbon, percent			*******	*******		******				0. 375 0. 052	0, 031	0.03		3. 23 0. 09
Manganese, percent										******		0. 54 17. 30		
				P	HYSIC	AL CH	RACT	ERISTI	CS 3				,	
Compression: Deformation limit, pounds per square inch Permanent set in 1 inch	30, 610	17, 530	11,000	10, 540	28, 385	26, 910	9, 430	7, 200	13, 880					
under 100,000 pounds per square inch Fension:	0. 136	0. 190	0.378	0. 268	0. 124	0. 185	3 0. 507	4 0. 544	0.320			********		*******
Yield point, pounds per square inch Tensile strength, pounds	(8)	19, 225	17, 330	18, 050	27, 630	28, 520	14, 355	14,000	18, 335	40, 865	39, 230	19,500-30,000	40, 335	
per square inch Elongation in 2 inches, per-		29, 590	18, 460	28, 820	77, 740	67, 660	21, 250	21,000	36, 670	69, 520		79, 000-93, 000	48, 590	********
Reduction in area, percent. Transverse tests:		1.00	1.75	11.00	28, 00	21.00	13, 00	10,00	33.00	34.00 51.00	35. 70	68. 0-70. 0 72. 0-75. 0	10. 17	
Deflection under 2,000 pound load, inches								*******						0.2
Breaking load, pounds			******						*****					2.9

- Chemical compositions shown are from analyses of materials used.
 All physical data for stainless steel obtained from manufacturer.
 Cracked at 90,070 pounds per square inch.
 Cracked at 97,800 pounds per square inch.
 None apparent before rupture.
 Proportional limit.

once more passed transversely across the specimen and back again, thereby subjecting all portions of the surface of the test plate to four additional longitudinal rollings. This finish removed practically all traces of the tool marks left by the planed finish.

C.R.—The cold-rolled finish as produced by the manufacturer of the plates.

M-A milled finish produced by using a spiral mill 4 inches in diameter, 5 inches long, with a 25 degree angle, 10 teeth, and a 10-inch rake. Operating at a spindle speed of 92 revolutions per minute, a lateral feed of 115 feet per minute, and a 1/64-inch cut, this mill produced a very smooth finish.

4. Direction of movement.—Three variations in direction of movement were used in these tests (fig. 1).

M₁—The direction of movement and the direction of finishing cuts of both plates were parallel.

M₂—The directions of finishing cuts of both plates

were parallel and the direction of movement of the plates was at right angles to the finishing cuts.

M3-The directions of the finishing cuts of the test plates were at right angles.

5. The effect of lubrication .- Selected combinations of plates were tested both with and without lubrication.

6. Effect of rust.—Cast iron specimens were exposed to weather until well rusted and then tested to determine the effect of rust.

7. Electrolysis.—The electrolytic action of stainless steel in contact with bronze and subjected to a salt solution and salt air was investigated.

Table 2 gives a summary of the conditions under which the tests were made.

PRECAUTIONS TAKEN TO INSURE EVEN APPLICATION OF BEARING PRESSURE AND THRUST

The coefficients of friction of the various materials were determined by means of a special apparatus designed and built by the Bureau. This device was used in conjunction with a universal testing machine and is shown schematically in figure 2. It consists essentially of a hydraulic jack for applying horizontal thrust, a calibrated beam for measuring this thrust, and the necessary steel framework for holding the various parts and the test specimens in their proper relative positions. Vertical loads or bearing pressures were applied by means of the universal testing machine, transmitted through two heavy car springs and a spherical bearing block. Two movable test plates, 4 by 4 by % inches, and two fixed plates, 4 by 41 by % inches, were used in each test. The two fixed plates were encircled by the steel frame, which supported the calibrated beam that served as a reaction for the hydraulic jack. The two movable plates were inset in the top and bottom of a cylindrical movable member, which was free to move under the thrust exerted by the hydraulic jack.

I b t I h n to

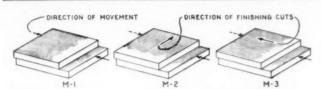


FIGURE 1.—RELATION OF DIRECTION OF MOVEMENT TO DIREC-TIONS OF FINISHING CUTS FOR BEARING PLATES TESTED.

Table 2 .- Materials and finishes used, direction of movement, and other test conditions

Combins mater			Fi	inishe	S 1150	ed			ection		Lubrication	Number of
A B C C D A A A A B B C C D A A B C C D C. S. S. M. I. I. C. C. S. R. B. E. E. P. B. E. E. P. B. B. 22 St. St. L. B. 22 St.	A B C D B C D D C C. S. C. S. R. S. S. L. L. E. L. B. 22 L. B. 17 L. B. B. 17 S. St. S. S. S. C. S. S. S. S. C. S. S. S. S. S. S. S. S. C. S. S. S. S. S. C. S. S. S. S. C. S. S. S. S. S. S. C. S. S. S. S. C. S. C. S.	Pc P	PM		144	R	C. R.	1 1 1 1 1 1 1		23		

Surfaces rusted.

Symbols apply to but 1.

e symbols used are explained as follows:

Metals:

moots used are explained as follows:
stals:

A = Bronze A, A. S. T. M. specification B22-21, class A.

B = Bronze B, A. S. T. M. specification B22-21, class B.

C = Bronze C, A. S. T. M. specification B22-21, class C.

C. I. = Cast iron, A. S. T. M. specification A32-24, class B.

C. S. = Cast steel, A. S. T. M. specification A32-24, class B medium.

D = Bronze D, A. S. T. M. specification B22-21, class D.

M. I. = Malleable iron, A. S. T. M. specification A47-30.

L. B. 17 = Lead bronze 22 percent.

L. B. 17 = Lead bronze 17 percent.

L. B. 8. = Lead bronze 8 percent.

P. B. E. = Phosphor bronze, A. S. T. M. specification B22-21, class A.

P. B. F. = Phosphor bronze, A. S. T. M. specification B22-21, class A.

R. S. = Rolled steel, A. S. T. M. specification B22-21, class B.

R. S. = Sainless steel,
nish:

uish;

PC=Coarse-planed finish.

PM=Medium-planed finish.

PF=Fine-planed finish.

M=Milled finish.

R=Rolled or planished finish.

C.R.=Cold-rolled finish as manufactured, rection of movement:

1—Movement and finishing cuts parallel.

2—Finishing cuts parallel, movement normal to direction of finishing cuts.

3—Finishing cuts at right angles.

brication:

The operation of the apparatus was as follows: The movable member with its two inset movable plates was placed between the two fixed plates. The desired bearing pressure was applied to the contact faces of the test plates by lowering the head of the testing machine. Horizontal thrust was then applied (by means of the hydraulic jack) to the movable member at a point midway between the contact faces of the two pairs of test plates (fig. 3). The magnitude of this thrust was

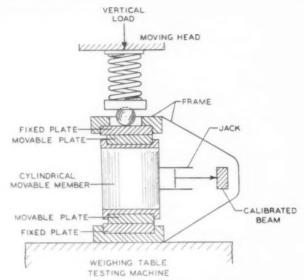


FIGURE 2.—SCHEMATIC DRAWING OF APPARATUS USED TO DETERMINE COEFFICIENT OF FRICTION.

indicated by the deflection of the calibrated beam. Since the two fixed plates were 1/2 inch longer, in the direction of thrust, than the two movable plates, it was possible for slip to occur and still maintain full contact between the faces.

The hydraulic jack was activated by a booster (a long-stroke, small-bore cylinder and piston) similar to those used in pressure lubrication, the system being first filled by means of a conventional hydraulic pump. The use of the booster to apply the final pressure to cause slip allowed a steady pressure to be applied without the pulsations usually caused by the strokes of a The interposition of the two heavy car springs between the head of the testing machine and the bearing blocks prevented oscillation of the beam of the testing machine during tests.

The deflection of the calibrated beam was measured by means of a micrometer dial graduated to 1/10000-inch divisions, one division on the dial being equivalent to 22 pounds of thrusting force. Inasmuch as the horizontal thrust measured by the calibrated beam was forced to overcome the friction existing between the contact faces of the two pairs of test plates under known unit bearing pressures, the thrust applied to each pair of plates was only one-half of that indicated by the dial reading.

The total thrusts required to overcome the initial frictional resistance under each of the unit bearing pressures were used in determining the coefficient of friction.

Definitions of the nomenclature used in this report are as follows:

Slip.—A single movement of the movable plates under lateral thrust while subject to some known bearing pressure was termed a slip.

Test.—A test comprised 15 sets of 20 slips, i. e., 300 independent slips under each of the unit bearing pressures used, other variables such as materials, finish, direction of movement, and state of lubrication being

Test series.—A test series is composed of all tests made of any one combination of materials under varying conditions of finish, direction of movement, and state of lubrication.

$\begin{array}{c} \textbf{INVESTIGATION INCLUDED STUDY OF UNLUBRICATED, LUBRICATED} \\ \textbf{AND RUSTED PLATES} \end{array}$

Tests of unlubricated plates.—In all tests the two movable plates were 4 by 4 by % inches and the two fixed plates were 4 by 4½ by % inches. In each test newly surfaced plates were used. Before testing, the plates were thoroughly washed in naphtha to remove surface grease, moisture, or any foreign matter. The plates were then inserted in the testing apparatus and a bearing load of 4,000 pounds (250 pounds per square inch, on the 16 square inches of contact area of the plates) was imposed by lowering the head of the testing machine. Thrust was then applied through the hydraulic jack by means of the booster until slip occurred. The point of slip was considered to be that point at which the needle of the micrometer dial started to recede. Successive thrusts were applied and readings noted until a succession of 20 slips had been recorded. Each set of 20 slips caused a shifting of the movable plates over the fixed plates of approximately 1/2 inch.

After each set, the plates were removed, rinsed in naphtha, turned horizontally through 180 degrees and replaced in the apparatus. The plates were thus kept free from lubricant and were subjected to sliding in opposite directions as would be the case in actual service. After 15 sets of 20 slips the bearing pressure was increasd to the next higher value. The schedule just described was carried out for bearing pressures of 250, 500, 750, and 1,000 pounds per square inch, respectively, and this constituted one test, the plates being resurfaced before being used again.

In every case where seizure was apparent the fact was noted, in order that the percentage of movements or slips in which seizure occurred during the course of each test might be determined. Seizure was determined either by audible chattering or by jumping of the plates as indicated by the micrometer dial. The thicknesses of all plates were measured by means of micrometer calipers at four points both before and after each test.

Tests of lubricated plates.—The procedure followed in making tests of lubricated plates was identical with that used in testing unlubricated plates with the following exceptions. After the newly surfaced plates were washed in naphtha a thin coating of graphite cup grease was applied to their contact faces. They were placed in the testing apparatus and a bearing pressure of 4,000 pounds, or 250 pounds per square inch, was applied. The plates were slid in successive slips once across the fixed plates to distribute the grease evenly and to force any excess from between the plates. The plates were then removed, reversed, and successive slips were made as in the tests of unlubricated plates, but with the original coating of lubricant intact.

Four cast-iron plates with the smooth-planed finish (PF) and four with a milled finish (M) were exposed to the weather, including snow and rain, for 76 and 56 days, respectively. This exposure produced a thick coating of rust. The plates were rubbed against each other with hand pressure to remove superficial rust and the friction tests were then made. The friction developed in both cases was so large that only the lowest unit bearing pressure (250 pounds per square inch) was applied. The plates were reversed between each set of 20 slips, and the rust loosened from the contact surfaces was lightly brushed off with a cloth between each series of slips. A comparison of the thick-

ness of these plates as measured before and after exposure to the weather and after friction tests had been completed indicated that the wear shown during the tests was caused by the loosening of surface rust, as no measurable reduction in original thickness was noted.

The following procedure was adopted in determining the coefficient of friction in each test. Curves were plotted for each of the four loadings, mean values of the total thrust necessary to overcome the friction existing on the 16 square inches of bearing surface, for each of the 15 sets of 20 slips, being used as ordinates, while the 15 sets were plotted at uniform spacings as abscissae.

COEFFICIENT OF FRICTION REMAINED CONSTANT UNDER VARIOUS BEARING PRESSURES

The averages of the mean values of thrust of the last 10 sets (200 individual slips) were used in determining the coefficient of friction, the first 5 sets being considered as adjusting or wearing-in values. These averages were plotted on abscissa, proportional to the bearing pressures and a mean curve was drawn through the resulting four points and the zero point. In all cases this curve was a straight line, which indicates that the value of the coefficient of friction remains constant under varying unit pressures. The maximum and minimum variations above and below the mean of any set of slips were shown by the limits of the vertical lines, drawn to scale, extending above and below the mean values as plotted.

It obviously being impracticable to reproduce the curves representing all tests performed in this investigation, typical curves developed in the manner just described are shown in figures 4, 5, 6, and 7. The results of all tests are compiled in table 3 in ascending order of coefficients of friction for tests without lubrication. In the column headed "Average maximum variations from mean thrust", the values shown were derived as follows: The average of the thrusting forces necessary to cause movement for the last 10 sets of slips, or of 200 individual slips, under a unit bearing pressure of 500 pounds per square inch, was used as a base. The maximum variations in thrusting force above and below the mean thrust for each of the last 10 sets of slips were averaged and these two averages expressed as plus or minus percentages of the base.

The values shown for the variations from mean thrust are for the 500 pounds per square inch unit pressure only, as this value is considered to be a representative value for all loadings. Variations for the tests of lubricated plates are omitted. In the majority of cases the variation for the lubricated plates was greater than in the case of unlubricated plates.

For the purpose of discussion, results for the 111 combinations tested, as arranged in table 3 and excluding the two tests of rusted plates (24-2 and 24-4) were arbitrarily divided into three equal groups of 37 combinations each. These groups are designated 1, 2, and 3, and contain the low, intermediate, and high values of the coefficient of friction, respectively.

In determining the effect of lubrication on the value of the coefficient of friction between flat plates, data from 77 tests both with and without lubrication were available for comparison. Examination of the individual curves for each of these 77 tests gave the following indications.

t e e f of

1 d-re

n-id of

mil-

Table 3 .- Coefficients of friction and other data for the various plates tested GROUP 1-LOW COEFFICIENTS OF FRICTION

				Coeffici		Average mum va from thrus	riations mean		Wear			Seizure-	-Percent:	age of slip	ps seized		
Series and test number 1	Metals used	Sur- face finish	Direc- tion of move- ment	Lubri-	No lubri-	pound square unit b pressu	is per e inch earing ire; no		No lubrica-	Lub	ricated— press		ring	No Iul	brication press	-Unit be	earing
				cated	cation	- lubric	eation —	catea	tion	250 pounds	500 pounds	750 pounds	1,000 pounds	250 pounds	500 pounds	750 pounds	1,000 pounds
17-1	C-R. S	PF	1		0, 106	Percent 2.1	Percent	Inches	Inches							Percent	Percent
35-1	L. B. 22-Stl. S C-C. S	P _M P _F	1 1		.110	4.0	2. 4 1. 4							*****		~	
36-1	C-Stl. 8	P _M	I		. 116	2.5	1.3				******		******	******	******		
17-2	C-R. S	M P _F	1	0.121	. 118	3. 2	1, 4										
15-7-8	B-R. S	M Pr	1	.110	. 127	1.1	1.5										
15-3-4 32-1	A-R. S	P _M Pc	1	. 122	, 128 , 128	1.7	1.9		0.001					******			
33-1	L. B. 17-L. B. 17.	Pc	1		. 130	1.0	2.7		/F=0	3							
30-1	P. B. EL. B. 22.	PM	1		. 132	3.3	1.7		M = .0005	,							
34-1 16-2	L. B. 8-L. B. 8 B-R. S	Pc M	1		. 132	1.4	1.4										
11-1-2		Pr	1	-	. 134	2.6	1.0		{A=0 C. 8,=.001	3							
6-1	A-C	PF	1		. 134	1.2	3.6	*****			******						
11-5-6	A-C. S D-R. S	R	1 1	. 123	. 135	2.9	1.3										
12-1	B-C. S	PF	1		. 136	1.0	2.4	******					*******		******		
18-1-2		Pc	1	. 121	. 137	1.4	.9		D=.001 R. S.=.002	}							******
3-3-4		P _M M	1	. 126	.137	1.3	1.3	******	*********	2	12	16	21				
15-1-2		1	1	. 116	. 138		1.2		A = .001 R. S. = .002	}							
1-7-8	A-A		1	. 126	. 138	1.4	2.7		(R. S.=.002								
8-1	A-B. B-C.	P _F	1		. 138	1.1	2.5										
4-19-20	D-D	. M	1	. 110	. 140	1.4	2.1	*****	*********		*******						
14-3-4	Λ-Λ	. Pr	1 2	. 162	. 143	3.1	1.9	Laneau.		19	31		18				
1-29-30 4-21-22	A-A D-D		3		. 146		1.2		********	*****							1
4-23-24	. D-D	. M	8	. 122	. 146	1.5	1.6					******					
9-1 3-9-10	. C-C	. R	i	7, 185		1.4	1.9				89	92	94	0	12	12	1
1-19-20 2-3-4	A-A B-B		1		. 148	1.1	1.8										
3-7-8	100				- 100												
	C-C	M	li				1.2			4	14	38	38				
		. M	li	. 164	. 150	1.1		1	EFFICIENT	1	-	1	38				
14-1-2	D-C. S	. PF		GR6	0. 150 0 UP 2-	1.1 INTER 0.9	MEDIA 2.1	TE CO	EFFICIENT	rs of I	FRICTIO	ON					
14-1-2 1-5-6 19-15-16	D-C, S	P _F Pc		GRG 0. 121 1. 139	0. 150 0. 150 0. 150	1.1 INTER 0.9 3.0	MEDIA 2. 1 1. 2	TE CO		rs of 1	FRICTIO	ON				12	3
14-1-2 1-5-6 19-15-16 24-3	D-C, S	PF PC M		GRO 1 0.121 3 .139 2 .136	0. 150 0UP 2— 0. 150 . 150 . 150	1.1 INTER	2. 1 1. 2 4. 5 4. 5	TE CO	0.001	rs of 1	FRICTIO	ON		0	1	. 39	33 22
14-1-2 1-5-6 19-15-16 24-3 1-11-12	D-C, S	P _F P _C M M P _M P _F		GR6 1 0.121 3 .139 2 .136	0. 150 0. 150 150 150 150 151 152	1.1 INTER 0.9 3.0 4.0 2.9 1.2 1.2	MEDIA 2. 1 1. 2 4. 5 4. 5 . 9 3. 0	TE CO	0.001	rs of I	FRICTIO	ON		0	1	. 39	
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-7-8 1-13-14	D-C. S	Pr Pc Pc M M Pm Pr Pm		GRG 1 0.121 3 .139 2 .136 3 .132 1 .148	0. 150 0. 150 . 150 . 150 . 151 . 152 . 152 . 152 . 152	1. 1 INTER 0. 9 3. 0 4. 0 2. 9 1. 2 2. 1. 5 2. 1. 0 2. 1. 3	2.1 1.2 4.5 4.5 9.3,0 2.0	TE CO	0.001	rs of I	FRICTIO	ON		. 0	1	. 39	
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-7-8 1-13-14 1-17-18	D-C. S	Pr Po M M Pr Pr Pr		GR6 GR6 1 0.121 3 139 2 136 1 3 132 1 148 1 128 3 134	0. 150 0. 150 150 150 151 152 152 152 153	1. 1 INTER 0. 9 3. 0 4. 0 2. 9 1. 2 1. 5 1. 0 1. 3 1. 1. 7	MEDIA 2.1 1.2 4.5 4.5 9.3.0 2.00 1.6 1.4	TE CO	0.001	rs of I	FRICTIO	ON		0	1	39	2
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-7-8 1-13-14 1-17-18 1-23-24 1-25-26	D-C, S	Pr Pc M M Pm Pr Pr Pr R		GRO GRO 1 0.121 3 .139 2 .136 3 .132 1 .148 1 .128 3 .134 1 .128 3 .134 1 .128	0. 150 OUP 2— 0. 150 . 150 . 150 . 151 . 152 . 152 . 152 . 154 . 154 . 154 . 154 . 154 . 154	1.1 INTER 0.9 3.0 4.0 2.9 1.2 1.5 2.1.5 1.7 1.7	MEDIA 2. 1 1. 2 4. 5 4. 5 9 3. 0 2. 0 1. 6 1. 4 1. 4 2. 3	TE CO	0.001	rs of I	FRICTIO	ON		0	1	39	2
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-7-8 1-13-14 1-17-18 1-23-24 1-25-26 24-1	D-C. S	P _F P _M P _M P _F P _F M R P _F P _F		GRG GRG 1 0.121 3 139 2 136 3 132 1 148 3 134 3 128 3 134 1 146	0. 150 OUP 2— 0. 150 . 150 . 150 . 150 . 151 . 152 . 152 . 152 . 154 . 154 . 157 . 157	1.1 INTER 0.9 0.3.0 0.2.9 0.2.9 1.2.2 1.5 2.1.0 2.1.3 1.7 4.1.7 7.4.2	MEDIA 2. 1 1. 2 4. 5 4. 5 9 3. 0 2. 0 1. 6 1. 4 1. 2 2. 3 4. 8	TE CO	0.001	rs of I	FRICTIO	ON		0	1	39	2
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-7-8 1-13-14 1-17-18 1-23-24 1-25-26 24-1 1-1-2 4-5-6	D-C. S	Pr Pc M M Pr		GRG GRG 1 0.121 3 .139 2 .136 3 .132 1 .148 4 .128 3 .134 3 .128 1 .146 1 .131	0. 150 OUP 2— 0. 150 . 150 . 150 . 150 . 151 . 152 . 152 . 154 . 154 . 157 . 157 . 157 . 157	1.1 INTER 0.9 0.3.0 0.4.0 0.2.9 1.2.2 1.5.2 1.0 1.7 7.1.7 7.4.2	MEDIA 2.1 1.2 4.5 4.5 9.3 0.0 1.6 1.4 2.3 4.8	TE CO	0.001 (F=0 (M=,002	rs of I	FRICTIO	ON		0	1	39	2
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-7-8 1-13-14 1-17-18 1-25-24 1-12-26 24-1 1-1-2 4-5-6 18-14	D-C. S	Pr Pc M R Pr Pc Pc Pc Pc Pc		GRO GRO 1 0.121 3 139 2 136 1 1-136 3 132 1 1-148 3 128 3 134 1 146 1 132 3 154	0. 150 0 UP 2— 0. 150 150 150 151 151 152 152 152 154 155 155 155 155 155 155 155 155 155	1.1 INTER 0.9 0.3.0 0.4.0 0.2.9 1.2.2 1.5 1.0 1.7 4.9 7 7 1.7 4.2 7 7 4.2 8 7.5 8 7.5 8 8 7.5 8 2.4	MEDIA 2.1 1.2 4.5 4.5 9 2.0 1.6 1.4 1.4 2.3 4.8 6.4 6.4 4.6 4.6 4.6 4.6 4.6 4.6 6.6 6.6	TE CO	- 0,001 - 0,001 - {F=0 M=,002,001	rs of I	FRICTIO	ON			1	39	2
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-7-8 1-13-14 1-17-18 1-25-26 24-1 1-1-2 4-5-6 18-14 3-5-6 25-7	D-C. S	PF PC MM PF		GRO 1 0.121 3 139 2 136 1 1.28 1 1.28 3 1.28 1 1.39 1 1.30 1 1.30 1 1.30 1 1.31 1 1.31	0. 150 0. 150 150 150 150 150 151 152 152 152 152 154 154 155 155 155 155 155 155 155 155	1.1 INTER 0.99 0.3.00 2.99 1.22 1.55 2.1.00 1.77 7.4.2 7.56 6.2.4 8.4.3	MEDIA 2.1 1.2 4.5 4.5 4.5 1.6 1.4 1.4 2.3 4.8 6.1 6.4 4.6 4.7 7.6 6.7	TE CO	(F=0 M=.002	rs of i	FRICTIO	ON			1	2 4	2
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-7-8 1-13-14 1-17-18 1-23-24 1-25-26 24-1 1-1-2 4-5-6 18-4 3-5-6 25-6 18-6	D-C, S	PF P P P P P P P P P P P P P P P P P P		GRO 1 0.121 3 139 2 136 1 1.48 1 1.28 3 134 3 128 1 1.46 1 1.33 1 1.34 1 1.31 1 1.31 1 1.31 1 1.31 1 1.31 1 1.31 1 1.31 1 1.31 1 1.31 1 1.31 1 1.31	0.150 0.150 1.50 1.50 1.50 1.50 1.50 1.5	1.1 INTER 0.99 0.3.0 0.2.99 1.2.2 1.5.5 2.1.0 1.7 7 7 4.2 7 7 4.2 7 7 6.2 1.4 8 6.2 4.4 8 6.1 6.4 8 6.1 6.2 6.1 6.1 6.1 6.1 6.1 6.1 6.1 6.1 6.1 6.1	MEDIA 2.1 1.2 4.5 4.5 4.5 4.5 4.6 1.4 4.6 2.3 4.8 4.6 4.6 4.7 7.6 7.6 2.6	TE CO	F=0 M=.002	TS OF I	FRICTIO	97	100		1	2 4	1
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-7-8 1-13-14 1-17-18 1-23-24 1-23-26 24-1 1-1-2 4-5-6 18-14 3-5-6 25-2 18-6 1-9-10	D-C, S	Presented Market		GR6 GR6 1 0.121 3 139 2 136 3 132 1 148 3 128 3 134 3 134 3 134 1 146 1 132 3 154 1 131 1 131 1 131 1 131 1 131 1 131	0.150 0.150 1.50 1.50 1.50 1.50 1.50 1.5	1.1 INTER. 0.9 0.9 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	MEDIA 2.1 1.2 4.5 4.5 5.0 2.0 2.0 1.6 1.4 1.4 2.3 4.5 6.1 6.4 6.4 6.4 6.4 6.4 7.6 7.6 7.6 8 7.5	TE CO	$\begin{cases} F=0 \\ M=.002 \\ .001 \end{cases}$	TS OF I	FRICTIO	97	100	0	1	2 4	1
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-7-8 1-13-14 1-17-18 1-23-24 1-25-26 24-1 1-1-2 4-5-6 18-4 3-5-6 25-7 18-6 1-9-10	D-C, S	PF P		GR6 GR6 1 0.121 1.139 2 136 3 .132 1 1.48 3 1.28 3 1.34 1 1.46 1 1.31	0. 150 0 UP 2— 0. 150 150 150 150 150 151 151 152 152 152 154 155 155 155 155 155 155 155 155 155	1.1 INTER 0.9 0.4 0.0 0.2 9 1.5 0.1 1.7 1.7 7 1.7 7 1.2 7 1.5 8 2.4 4.2 1.2 2.1 1.7 2	MEDIA 2.1 1.2 4.5 4.5 4.5 9.3 0.0 2.0 0.1 6.1 1.4 9.2 4.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8 9	TE CO	$\begin{cases} F=0 \\ M=.002 \\ .001 \end{cases}$	TS OF I	FRICTIO	97	100	0	5 97	24 98	1
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-7-8 1-13-14 1-17-18 1-23-24 1-25-26 24-1 1-1-2 4-5-6 18-14 3-5-6 18-14 3-5-6 19-10 25-2 18-6 1-9-10 2-1-9	D-C. S	- M		GRO 1 0.121 3 139 2 136 1 1 1.28 3 134 3 128 4 1.28 3 134 1 146 1 132 1 131 1 118 2 136 1 1 118	0. 150 0 UP 2— 0. 150 150 150 150 150 150 150 150 150 150	1.1 INTER. 0.9 0.9 0.0 4.0 0.0 2.9 0.0 1.2 1.3 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	MEDIA 2.1 1.2 4.5 4.5 4.5 9.0 1.6 1.6 1.4 2.1 1.4 2.6 1.4 2.6 1.5 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8	TE CO	$\begin{cases} F=0 \\ M=.002 \\ .001 \end{cases}$	TS OF I	FRICTIO	97	100		5 97	24 98	1
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-7-8 1-17-18 1-33-24 1-17-18 1-33-24 1-4-5-6 18-1-4 1-1-2 4-5-6 18-1-4 1-1-2 1	D-C. S. A-A. C. S. C. S. C. S. C. S. C. S. C. IC. I. A-A. A-A. A-A. A-A. C. IC. I. A-A. D-D. D-B. S. C. C. S. M. I. D-B. S. A-A. B-B. B-B. M. IM. I. A-A. C. S. C.	PF PC PF PF PF PF PF PF		GR6 GR6 GR6 1 0.121 1.139 2 136 3 132 1 148 3 128 3 134 1 146 1 131 1 131 1 131 1 131 1 141 1 141 1 151 1 152 1 152 1 152 1 153	0. 150 0 UP 2— 0. 150 150 150 150 150 151 151 152 152 152 153 155 155 155 155 155 155 155 155 155	1.1 INTER. 0.9 0.9 0.4 0.0 0.4 0.0 0.9 0.1 1.2 2.1 1.5 2.1 1.7 7.1 7.7 1.7 7.4 2.2 1.3 0.9 1.6 1.4 1.7 1.7 7.1	MEDIA 2.1 1.2 4.5 4.5 3.0 3.0 1.6 1.4 1.4 2.3 4.6 4.6 4.6 4.7 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7	TE CO	$\begin{cases} \mathbf{F} = 0 \\ \mathbf{M} = .002 \\ .001 \end{cases}$	TS OF I	FRICTIO	97	100	0	5 5 97	24 98 45	1
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-78 1-13-24 1-23-24 1-23-24 1-23-26 24-1 1-1-2 4-5-6 18-14 1-2-6 25-2 18-6 25-2 18-6 25-2 18-6 25-2 18-6 25-2 18-6 25-1 1-9-10 2-1-1 2-1 2	D-C. S. A-A. C. S. C. S. C. S. C. S. C. S. C. IC. I. A-A. A-A. A-A. A-A. C. IC. I. A-A. D-D. D-B. S. C. C. S. M. I. D-B. S. A-A. B-B. B-B. M. IM. I. A-A. C. S. C.	Pr Pr Pr Pr Pr Pr Pr Pr	R.	GR6 GR6 1 0.121 3 139 2 136 3 .132 1 .148 3 128 4 128 3 134 1 .146 1 .132 3 154 1 .141 1 .131 1 .155	0. 150 OUP 2— 0. 150 .150 .150 .150 .151 .151 .152 .152 .152 .154 .155 .155 .155 .155 .155 .155 .155	1.1 INTER. 0.9 0.9 0.4 0.0 0.4 0.0 0.9 0.1 1.2 2.1 1.5 2.1 1.7 7.1 7.7 1.7 7.1 7.7 1.7 7.1 2.2 1.3 0.9 1.2 2.3 1.3 1.1 1.7 2.2 2.5 2.2 2.3 1.3 1.3 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	MEDIA 2.1 1.2 4.5 4.5 5.0 3.0 6.1 1.4 7.2 3.8 4.5 6.4 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.6	TE CO	(F=0 M=.002 (F=0 M=.001 (F=0	TS OF I	FRICTIO	97 57	100	96	55	24 98 45	1
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-7-8 1-13-14 1-17-18 1-23-24 1-23-24 1-23-26 24-1 1-1-2 4-5-6 18-4 3-5-6 19-10 25-7 18-6 1-9-10 2-1-12 2-1-2 1-2-12 1-	D-C. S. A-A. C. SC. S. C. IC. I. A-A. A-D. D-D. A-A. A-A. A-A. C. IC. I. A-A. D-D. D-R. S. C-C. C. SM. I. D-R. S. A-A. B-B. B-B. M. IM. I. A-A. C. SC. S. P. B. FP. B. I. D-D. A-A.	Pr Pr Pr Pr Pr Pr Pr Pr	R.	GR6 GR6 1 0.121 3 139 2 136 3 .132 1 .28 3 128 1 .146 1 .39 1 .151 1 .118 2 .136 1 .148 1 .132 3 1.141 1 .118 2 .136 1 .144 1 .155 1 .151 2 .122 3 .141 1 .151	0. 150 OUP 2— 0. 150 .150 .150 .150 .151 .151 .152 .152 .152 .154 .155 .155 .155 .155 .155 .155 .155	1.1 INTER 0.9 0.4 0.0 0.9 1.2 1.0 1.2 1.0 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	MEDIA 2.1 1.2 4.5 4.5 4.5 9.0 1.6 1.4 1.4 2.4 1.4 2.6 1.7 7.6 1.6 1.7 7.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1	TE CO	F=0 M=.002 .001 .001	73 OF I	81 81 81	97 57	100	0 96	5 5 97	24 98 45	1
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-7-8 1-13-14 1-17-18 1-23-24 1-23-24 1-23-24 1-25-26 24-1 1-1-2 4-5-6 18-4 3-5-6 19-10 25-7 18-6 1-9-10 2-1-12 2-1-2 1-2-12 1	D-C, S. A-A. C, SC, S. C, LC, I. A-A. A-A. A-A. A-A. C, IC I. A-A. D-D. D-R, S. C-C. C, SM, I. D-R, S. A-A. B-B. B-B. M, IM, I. A-A. C, SC, S. P, B, FP, B, I. D-D. D-D. D-D. D-D. D-R, S. A-A. B-B. B-B. M, IM, I. A-A. C, SC, S. D-D. D-D. D-D. D-D. D-D. D-D. D-D. D-	PF PC PC PF PF PF PF PF	R.	GRO 1 0.121 3 139 2 136 1 1.28 3 132 4 1.28 3 134 4 1.28 3 128 3 128 4 1.34 1 1.46 1 1.32 1 1.41 1 1.11 2 1.33 1 1.41 1 1.15 1 1.51 1 1.51 1 1.51 1 1.51 1 1.51 2 1.22 1 1.33 1 1.44 1 1.34	0. 150 0 UP 2— 0. 150 150 150 150 150 150 150 150 150 150	1.1 INTER. 0.9 0.9 0.0 4.0 0.0 4.0 0.0 2.9 1.2 2.1 0.0 2.1 1.7 4.2 2.1 1.7 4.2 2.1 1.7 4.2 2.1 1.6 5.1 1.2 1.6 5.1 1.6 5.1 1.7	MEDIA 2.1 1.2 2.1 1.2 4.5 4.5 4.5 4.5 4.5 4.6 4.6 4.6 4.6 4.6 4.6 4.6 4.6 4.6 4.6	TE CO	F=0 M=.001 (M) (M)	73	81 81 48	97 5 57	1000	0 96	5 5 97	24 98 45	1
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-7-8 1-13-14 1-17-18 1-25-26 24-1 1-1-2 4-5-6 18-14 3-5-6 25-2 18-6 1-9-10 2-1-1 2-1-1 2-1-1 2-1-1 2-1-1 2-1-1 2-1-1 2-1-1 1-1-1 2-1-1 1-	D-C. S. A-A. C. SC. S. C. LC. I. A-A. A-D. D-D. A-A. A-A. A-A. A-A. A-A	Pr Pr Pr Pr Pr Pr Pr Pr	R.	GR6 GR6 1 0.121 3 139 2 136 1 1.28 3 132 1 1.48 1 1.28 3 134 3 134 1 1.46 1 1.31 1 1.11 1 1.15 2 1.32 1 1.44 1 1.15 2 1.22 1 1.33 1 1.44 1 1.15 2 1.22 1 1.33 1 1.44 1 1.35 1 1	0. 150 OUP 2— 0. 150 150 150 150 150 150 151 152 152 153 155 155 156 156 156 166 166 166 166 166	1.1 INTER. 0.9 0.9 0.0 4.0 0.0	MEDIA 2.1 1.2 4.5 4.5 4.5 9.0 2.0 1.6 1.4 1.4 2.4 1.4 2.6 1.5 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	TE CO	(F=0 \ M=.001 M=.001 M=.001	73	81 81 48	97 5 57	1000	96	1 5 97	24 98 45 35 60	3
14-1-2 1-5-6 19-15-16 19-15-16 24-3 1-11-12 47-8 1-13-14 1-13-14 1-13-24 1-1-2-26 24-1 1-1-2-26 18-1-4 3-5-6 25-1 19-6 19-1-12 22-1-2 19-1-12 22-1-2 19-1-12 23-1-18 31-18 31-18 3	D-C. S. A-A. C. S. C. S. C. S. C. S. C. IC. I. A-A. A-A. A-A. A-A. C. IC. I. A-A. D-D. D-R. S. C. C. SM. I. D-R. S. A-A. B-B. B-B. M. IM. I. A-A. C. S. C. S. P. B. FP. B. F. D-D. A-A. C. S. C. S. D-D. D-D. B-B. B-B. C. S. M. I. D-D. B. B-B. C. S. M. I. D-D. D. B. FP. B. FP. B. F. D-D. B. B-B. C. S. M. I. D-D. D. B. FP. B. FP. B. F. D-D. B. FP.	Pr Pr Pr Pr Pr Pr Pr Pr	R.	GRO 1 0.121 3 139 2 136 1 1.28 3 134 1 1.28 3 134 1 1.46 1 1.31 2 1.36 1 1.31	0. 150 0 UP 2— 0. 150 150 150 150 150 150 150 150 150 150	1.1 INTER 0.9 0.4 0.0 0.2 9 1.2 1.5 1.0 0.2 1.3 1.7 1.7 1.7 1.7 1.5 5.7 1.5 5.5 1.5 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	MEDIA 2.1 1.2 2.1 1.2 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5	TE CO	(F=0 \ M=.001 M=.001 M=.001	73 OF I	81 81 48	97 5 57	1000	96	5 5 97 4 5 5 5 5 97	24 98 45 0 35 44 45 3 44 45 3 4 44 45 3 4 45 4 45	2
14-1-2 1-5-6 19-15-16 24-3 1-11-12 24-3 1-11-12 24-1 1-17-18 1-33-24 1-1-25-26 24-1 1-1-25-26 24-1 1-1-25-26 24-1 1-25-26 22-1 1-2-5-1 22-5-1 22-5-1 22-5-1 22-1 1-2-2	D-C. S. A-A. C. SC. S. C. IC. I. A-A. A-A. A-A. A-A. A-A. C. IC I. A-A. D-D. D-R. S. C-C. C. SM. I. D-R. S. A-A. A-A. C. JW. I. D-B. B-B. B-B. M. IM. I. A-A. C. SC. S. P. B. FP. B. F. D-D. B-B. C. S. C-D. D-D. B-B. C. S. C.	Pr Pr Pr Pr Pr Pr Pr Pr	R.	GR6 GR6 1 0.121 3 139 2 136 1 1.28 3 132 1 1.48 1 1.28 3 134 1 1.46 1 1.31 1 1.18 2 1.34 1 1.15 1 1.15 1 1.15 2 1.22 1 1.33 1 1.44 1 1.35 1 1.34 1 1.35 1	0. 150 0 UP 2— 0. 150 150 150 150 150 150 150 150 150 150	1.1 INTER. 0.9 0.3 0.0 4.0 0.0 4.0 0.0 4.0 0.0 4.0 0.0 2.9 0.0 1.2 0.0	MEDIA 2.1 1.2 2.1 1.2 4.5 4.5 4.5 4.5 4.6 1.4 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4	TE CO	F=0 M=.001 (M=.001)	73 OF I	81 81 81	97 57	100	96	5 5 97 4 6 9 10 11	24 98 45 98 45 98	2
14-1-2 1-5-6 19-15-16 24-3 1-11-12 7-1 4-78 1-13-14 1-17-18 1-25-26 24-1 1-1-2 4-5-6 18-14 1-2-26 24-1 1-1-2 18-6 18-4 3-5-6 18-4 1-2-1 18-6 19-10 2-1-1 2-1-1 2-1-1 1-2-1 2-1-1 2-1-1 1-1-1 1-1-1 1-2-2 1-1-1 2-1-1 2-1-1 2-1-1 1-1-1	D-C. S. A-A. C. SC. S. C. IC. I. A-A. A-A. A-A. A-A. D-D. A-A. A-A. C. IC. I. A-A. D-D. B-R. S. C-C. C. SM. I. D-R. S. A-A. C. SC. S. B-B. B-B. M. IM. I. A-A. C. SC. S. P. B. FP. B. I. D-D. D-D. B-B. C. SM. I. D-D. D-D. D-D. B-B. C. SM. I. D-D. D-D. D-D. B-B. C. SM. I. D-D. D-D. D-D. D-D. D-D. D-D. D-D. D-	Pr Pr Pr Pr Pr Pr Pr Pr	R.	GR6 GR6 GR6 1 0.121 3 139 3 136 1 128 3 134 3 128 3 134 3 134 1 140 1 151 1 151 2 136 1 144 1 151 1 151 2 121 1 133 1 144 1 1 151 2 121 1 133 1 144 1 1 151 2 121 1 133 1 144 1 1 155 2 122 1 124 1 1 133 1 144 1 1 133 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0. 150 0 UP 2— 0. 150 150 150 150 150 150 150 150 150 150	1.1 INTER. 0.9 0.9 0.0 4.0 0.0 4.0 0.0 2.9 0.0 1.2 1.0 0.2 1.0	MEDIA 2.1 1.2 2.1 1.2 3.0 3.0 3.0 3.0 3.0 3.0 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8	TE CO	F=0 M=.001 (00) F=0 M=.001	73 OF I	81 81 81	97 57	100	96	5 597 977 4 6 6 6	24 98 35 35 600 100 100 100 100 100	2

First number indicates series; remaining numbers indicate individual tests. Where 2 test numbers are shown, they refer to tests of lubricated and unlubricated plates respectively.

Lubricant removed, coefficient of friction dropped to 0.170.
Lubricant removed, coefficient of friction dropped to 0.152.

Table 3 .- Coefficients of friction and other data for the various plates tested-Continued Choup a High competations of anighton

				Coeffici		A verage mum var from r thrust	riations nean	,	Wear			Seizure-	-Percent	age of slip	os seized		
Series and test number	Metals used	Sur- face finish	Direction of move- ment	Lubri-	No lubri-	pound square unit be pressu	s per inch earing re; no		No lubrica-	Lub	ricated— press		ring	No lui	press		earing
				cated	cation	lubrie +	ation -	cated	tion	250 pounds	500 pounds	750 pounds	1,000 pounds	250 pounds	500 pounds	750 pounds	1,000 pound
1-17-18	R. SR. S	м	3	0. 141	0. 174	Percent 13. 2	Percent 12.0	Inches	Inches	Percent	Percent	Percent	Percent	Percent 19	Percent 43	Percent 42	Percen 7
-5-6	D-C. S. C. SC. S.	R Pc	1	110	. 174	2.5 8.7	5. 1 3. 2	0,001	0.002	0	B	10	26	1	1	2	1
3-1	M. IC. I	Pr	1		. 174	2.0	4.6		M. I. = . (01 C. I. = 0	}				0	0	18	
-2	M. IC. I	M	1		. 174	6.8	2.2									******	
-15-16	P. B. EP. B. E R. SR. S.	P _M M	3 2	. 140	. 175	2. 2 17. 1	12.1							34	8 41	82 75	
⊢3-4 ⊢5-6	M. IM. I C. SR. S	M	1	. 135	. 178	8.6	5. 9 7. 8							31	40 76	49 75	
-2	R. SM. I	M	1	. 130	. 182	7.5	5.3							52	63	78	
-13-14	R. SM. I C. SC. S		1	. 131	. 183	14.8 12.2	9. 6 7. 4		. 001					43	62 55	77 76	
-11-12	C. SC. S	Pr	3	. 145	. 187	19.8	10, 6						2	42	69	83	
-15-16	D-D		2	. 162	. 190	4.0	5. 5		(F=.001	} 10		22	44	15	46	78 54	
-29-30	D-D	Pc R	3	. 150	. 190	16.7	13. 4	100.	${ m F} = .001 { m M} = .002$	10	14	22	41	0	26	63	
9-1	P. B. EP. B. E.	C. R	. 1		. 195	8.4	7.6							. 0	2	3	
9-9-10 6-2	C. SC. S C. SC. I	Py	2	. 141	. 198	17.8	9.9							29	87 18	91 58	
-17-18	D-D		3	. 176	. 204	5.4	10. 4	f F = 0)					6	57	61	
0-1-2	C. SR. S		1	. 160		13.0	9. 7	UM=.001		10	10	21	30		37	35	
1-5-6	D-D R. SR. S	Pr	1 3	. 144	. 210	4.7 17.9	9.5		.001			43		63	78 56	84	
21-13-14	R. SR. S	M	1	. 134	. 215	15.0	17.6		.001		10	40		_ 23	48	77	
9-7-8	C. SC. S R. SR. S	PF	1	. 140			15.3			39	68	72	76	. 54 80	81	90	
6-1	C. SC. I	Py	1	. 200	district the same of the same		17.2							70	78	89	
1-1-2		. Pc	1	. 154	. 224	16.8	16.0	F=0 M=.00	.001	6	15	26	35	19	59	66	
20-3-4			1	. 160	, 238	17.4	16.8		(C. I.=0	- 6	26	52	63	94	93	97	
28-2			1		. 239	1	4.8		R. S. = .001					- 81	86	93	1-4
21-9-10	R. SR. S	P _F	2													81 98	
28-1	1					1	1		fC. L=0	1				87	1	1	
1-3-4	Α-Α	Po	2	. 320	. 390	Se	eized		(R. S.=.001	100				. 100			
19-3-4 4-3-4	C. SC. S D-D.	Pc Pc					eized eized	, 001		92				100			
21-3-4							eized	j F =0	F=0 1 M=.001	} 100				100			
	1	-	1	1		TEST	S OF R	USTEL	PLATES		-				-		
24-4	C. IC. I	M		1	4.48	1	eized	1	8.00		1	ī	1	100		1	

**Rust only wore off, no decrease in original thickness.

The symbols used are explained as follows:

Metals—

A = Bronze, A. S. T. M. Specification B22-21, class A.

B = Bronze, A. S. T. M. Specification B22-21, class B.

C = Bronze, A. S. T. M. Specification B22-21, class C.

C. I. = Cast iron, A. S. T. M. Specification A48-29, heavy.

C. S. = Cast steel, A. S. T. M. Specification A27-24, class B medium.

D = Bronze, A. S. T. M. Specification B22-21, class D.

L. B. 22 = Lead bronze-22 percent lead.

L. B. 17 = Lead bronze-17 percent lead.

Direction of measurement.

Direction of movement-

rection of movement— $1 = Direction\ cf$ movement and direction of finishing cuts parallel. $2 = Direction\ of\ movement\ at\ right\ angles\ to\ finishing\ cuts,\ finishing\ cuts\ parallel.$ $3 = Direction\ of\ the\ finishing\ cuts\ at\ right\ angles.$

In 60 tests of unlubricated plates the mean values of the coefficient of friction, for the last 10 sets of slips under each of the four loads, showed a tendency to remain constant or to decrease slightly, and in 17 tests this value showed a tendency to increase slightly, while in the tests of lubricated plates this value for 44 remained constant or decreased and 33 showed a marked tendency to increase.

Metals—Continued.

M. I. = Malleable ircn, A. S. T. M. Specification A47-30.

P. B. E. = Phosphor bronze, A. S. T. M. Specification B22-21, class Λ. P. B. F. = Phosphor bronze, A. S. T. M. Specification B22-21, class B. R. S. = Rolled steel, A. S. T. M. Specification A7-29, structural grade. Sti. S. = Stainless steel.

Wear - M=Movable plate F=Fixed plate.

Figure 7 shows data from one of the tests in which this tendency for the resistance to increase as the test progressed is evident. The example given is a typical rather than an extreme case.

In four tests (1-15-16, 3-5-6, 3-7-8, and 3-9-10) the lubricated plates showed greater friction than the unlubricated plates, and in all four cases the lubricated plates seized while unlubricated plates seized in only

⁴ Surfaces rusted by exposure 4 Rust only wore off, no decrease in original thickness.

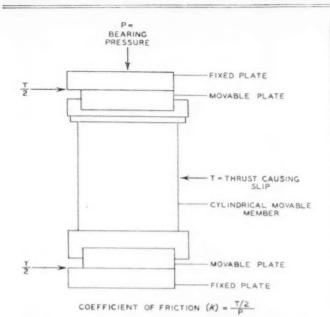


FIGURE 3.—ARRANGEMENT OF BEARING PLATES DURING TEST, SHOWING THE FORCES INVOLVED IN CALCULATING THE COEFFICIENT OF FRICTION (k).

one case. In two tests (3-5-6 and 3-9-10), where the friction with lubrication was greater than without lubrication, all lubricant was washed off with naphtha at the end of the tests and a single set of 20 slips under each of the four loadings was run without lubricant. These results showed a definite decrease in the coefficients of friction (from 0.190 and 0.185, when lubricated, to 0.152 and 0.170, respectively) with no lubrication.

In group 1 of table 3 there were 21 combinations that were tested both with and without lubrication. Of these 21 combinations, the coefficients of friction of the lubricated plates in 6 cases showed a tendency to increase and in 15 cases a tendency to remain constant as the tests progressed, while in the same 21 combinations, where unlubricated plates were used, only 2 cases showed a tendency to increase, 16 remained constant, and 3 decreased.

In group 2 of table 3 there were 29 combinations available for a similar comparison. In these 29 tests the tendencies of the coefficients of friction to vary were as follows: When lubricated plates were used, 18 showed a tendency to increase, 10 to remain constant, and 1 to decrease. With no lubrication, 3 combinations showed a tendency to increase, 23 to remain constant, and 3 to decrease.

In group 3 of table 3, 27 combinations were available for comparison and the following tendencies to vary were noted. With lubricated plates 9 combinations showed a tendency to increase, 17 to remain constant, and 1 to decrease. With the unlubricated plates, 12 combinations showed a tendency to increase, 12 to remain constant, and 3 to decrease.

LUBRICANT OF QUESTIONABLE PERMANENT VALUE IN REDUCING FRICTION

d

Considering groups 1 and 2, as comprising the most desirable combinations, table 4 shows the general tendencies of the coefficients to vary and permits a

comparison to be made between the lubricated and unlubricated plates in this respect.

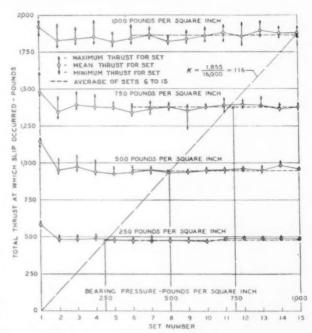


FIGURE 4.—RELATIONS BETWEEN BEARING PRESSURE AND THRUST AT WHICH SLIP OCCURRED FOR TEST SERIES 36, No. 1, Showing Derivation of Coefficient of Friction (k): BRONZE C ON STAINLESS STEEL; MEDIUM-PLANED FINISH; MOVEMENT PARALLEL TO FINISHING CUTS; NO LUBRICATION; NO WEAR; AND NO SEIZURE.

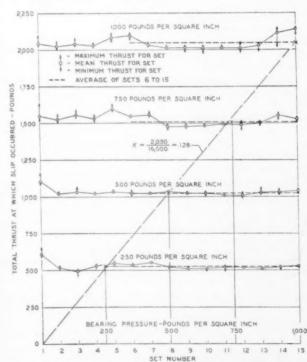


FIGURE 5.—RELATIONS BETWEEN BEARING PRESSURE AND THRUST AT WHICH SLIP OCCURRED FOR TEST SERIES 16, No. 1.
BRONZE B ON ROLLED STEEL; FINE-PLANED FINISH; MOVEMENT PARALLEL TO FINISHING CUTS; NO LUBRICATION; NO WEAR; AND NO SEIZURE.

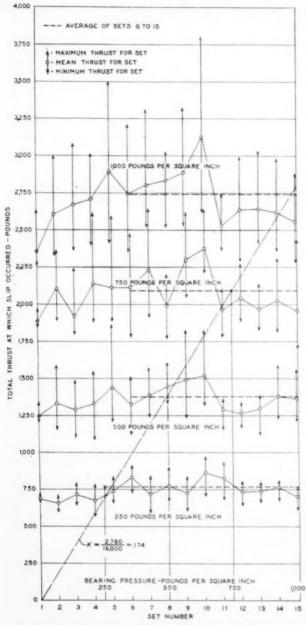


FIGURE 6.—RELATIONS BETWEEN BEARING PRESSURE AND THRUST AT WHICH SLIP OCCURRED FOR TEST SERIES 21, No. 17. ROLLED STEEL ON ROLLED STEEL; MILLED FINISH; MOVEMENT—FINISHING CUTS AT RIGHT ANGLES; NO LUBRICATION; NO WEAR; SEIZURE AT 250 POUNDS PER SQUARE INCH, 19 PERCENT of SLIPS; AT 500 POUNDS, 43 PERCENT; AT 750 POUNDS, 42 PERCENT; AND AT 1,000 POUNDS PER SQUARE INCH, 70 PERCENT OF SLIPS.

Table 4.—Variations in coefficient of friction in tests of lubricated and unlubricated plates

Condition of plates	Variation in coefficient of friction during last 20 sets of slips						
	Constant	Increased	Decreased				
UnlubricatedLubricated	Number of tests 39 25	Number of tests 5 24	Number of tests				

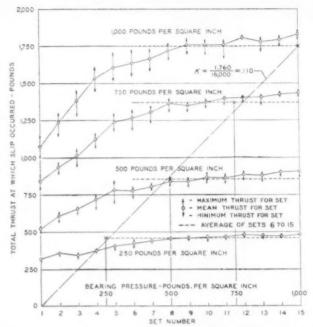


FIGURE 7.—RELATIONS BETWEEN BEARING PRESSURE AND THRUST AT WHICH SLIP OCCURRED FOR TEST SERIES 14, No. 6. BRONZE D ON CAST STEEL; ROLLED OR PLANISHED FINISH; MOVEMENT PARALLEL TO FINISHING CUTS; PLATES LUBRICATED; NO WEAR; AND NO SEIZURE.

In group 1, the values for the lubricated plates are on an average 11.5 percent less than the values for the unlubricated plates, while in groups 2 and 3 the differences in favor of the lubricated plates are 13.8 percent and 28.3 percent, respectively.

It appears that, although lubrication with the type of lubricant used causes an initial decrease in friction, with continued movement the lubricant is forced out from between the plates and the friction increases until it may equal or surpass that of the unlubricated plates. The smoother the finish, the sooner the beneficial effects of lubrication appear to be dissipated.

Inasmuch as the beneficial effects of lubrication for the most desirable combinations (groups 1 and 2) are small and since in many of the tests these effects decreased during the comparatively limited number of movements made in a test, it seems probable that the use of a single application of graphite grease, or other lubricant which will flow, is of but little, if any, permanent value when used between 'lat plates subject to load intensities such as used in these tests.

In considering the effects of surface finish on friction, 19 groups of tests with machined surfaces are available for comparison. In making the comparison, tests of unlubricated plates, with direction of movement and direction of finishing cuts parallel, were used. The results of these tests are assembled in table 5 in four groups:

- 1. Like metals (ferrous).
- 2. Unlike metals (ferrous).
- 3. Like metals (bronze).
- 4. Unlike metals (ferrous and bronze).

In groups 1 and 2 the fine-planed finish gave the highest values of the coefficient of friction and the milled finish gave the lowest values except in the case of cast iron on cast iron, for which the lowest value was

Table 5.—Effect of surface finish on magnitude of coefficient of friction; all plates unlubricated; direction of movement and direction of finish parallel

GROUP 1-LIKE METALS-FERROUS

Metals	Finish	Coefficient of friction (k)	Seizure
R, S	Pr	0. 266	Yes.
	Pc	. 224	Yes.
	M	. 215	Yes.
C, S	Pr	. 218	Yes.
	M	. 186	Yes.
	Pc	. 174	Yes.
C. I	PF	. 157	Yes.
	M	. 150	Yes.

GROUP 2-UNLIKE METALS-FERROUS

R. SC. I	I Pr	0. 275	Yes.
k, DV. L	M P-	. 239	Yes. Yes.
C. SR. S	$-\left\{\begin{array}{c} \mathbf{P_F} \\ \mathbf{M} \\ \mathbf{P_F} \\ \mathbf{P_C} \\ \mathbf{M} \end{array}\right.$. 208	Yes.
SC. I	PF	, 220	Yes.
R. SM. L	PF	. 203	Yes. Yes.
M. IC. I	P _P	. 182	Yes. Yes.
	M Pr	. 174	No. Yes.
C. SM. I	- M	. 158	Yes.

GROUP 3-LIKE METALS-BRONZE

	P _F	0. 210	Yes. No.
	Pc	. 163	No.
		. 152	No.
	P _M M		No.
1	21	. 140	
	R	. 172	Yes.
	M	. 167	No.
	PF	. 162	No.
	Pc	. 161	No.
	PM	. 150	No.
	Pc	. 172	No.
	Pr	. 158	No.
	P _F M	. 150	No.
	R	. 148	Yes.
	PM	. 137	No.
	Pc	. 157	No.
	R	. 157	No.
	D-	. 152	No.
)	P _F M		No.
	D.	. 148	
	P _M	. 138	No.

GROUP 4-UNLIKE METALS-FERROUS AND BRONZE

	1		
	R	0. 174	No.
D-C. S	P _F M	. 150	No.
	M	. 140	No.
	P _F P _M	. 159	No.
)-R. 8	PM	. 158	No.
	P _C M	. 137	No.
		. 135	No.
	Pc	. 138	No.
I-H, S	PM	. 128	No.
	M	. 127	No.
	P _F M R	. 123	No.
i-C. S	M	. 138	No.
	R	. 135	No.
	Pr M	. 134	No.
B-R. S	M	. 132	No.
	Pr	. 128	No.
C-R. S	M	. 118	No.
	Pr	. 106	No.

Symbols used are:

A = Bronze A.
B = Bronze B.
C = Bronze C.

C. I.=Cast iron.
C. S.=Cast steel.
M. I.=Malleable iron.
R. S.=Rolled steel.

given by the coarse-planed finish. Seizure was noted in 100 percent of the tests in group 1 and 92 percent of those in group 2.

In group 3 either the medium-planed or the milled finishes had the lowest values of the coefficient of friction. Seizure was noted in only 15 percent of the 20 tests comprising this group.

In group 4 the fine-planed and milled finishes gave the most satisfactory results. No seizure was noted in this group.

Tests were made of combinations of two grades of cold-rolled phosphor bronze, with surfaces as rolled at the mill. In both cases the direction of movement and the directions of finish of all plates were parallel. Phosphor bronze E showed a high coefficient of friction, falling within the highest 20 percent of all tests made. Seizure was noted in 6 percent of the slips under the maximum loads. Phosphor bronze F, under similar conditions of test, gave a coefficient of friction within the higher 50 percent of all tests made, and no seizure was noted.

An attempt to determine the comparative merits of a cold-rolled finish and a machined finish was later made. The cold-rolled phosphor bronze specimens, both E and F, were machined with a medium-planed finish (P_M) and tested in like pairs. No lubrication was used and tests were made with the direction of the finishing cuts of the contact faces at right angles (M_3) . Data from former tests indicated the above finish and direction of movement to be satisfactory for use with like bronzes.

The results of these tests (series 29 and 31) are shown in the general compilation of test results in table 3. By comparing the results it will be seen that no wear was apparent in any of these tests. In the case of phosphor bronze E, the machined surfaces showed a 10-percent decrease in friction when compared with the cold-rolled finish, while in the case of phosphor bronze F the machined plates showed approximately a 5-percent increase in friction in comparison with the cold-rolled plates. Both materials, when tested with machined surfaces, showed a marked increase in the number of slips which seized, from a maximum of 6 percent to 87 percent in series 29 and from a maximum of 0 percent to 89 percent in series 31. However, the intensity of seizure, as evidenced by the lack of violence of the jump and the small distances moved under lateral thrust, was low in both tests. The percentage of maximum variation from the mean thrust at slip was lower when machined surfaces were used than when cold-rolled surfaces were used.

If due consideration is given to the variations from the mean thrust necessary to cause slip found in the several tests, and to the limited number of comparisons made for the two finishes, the limited differences in coefficient of friction found indicate no marked superiority for either finish.

MILLED FINISH WITH FINISHING CUTS AT RIGHT ANGLES FOUND MOST SATISFACTORY

Two tests were made of cast-iron plates, one with a fine-planed surface and one with a milled finish, all surfaces rusted by exposure to weather. The friction developed was excessive in both series and only under the lowest unit bearing pressure used (250 pounds per square inch) could slipping be produced.

From the results shown in table 5 the following conclusions seem reasonable:

1. A milled finish is most satisfactory when ferrous materials are used in combination.

2. A milled or medium-planed finish is most satisfactory for combinations of like bronzes.

3. A milled or fine-planed finish is most satisfactory for combinations of ferrous materials with bronzes.

In connection with these conclusions, it should be remarked that the spread of values resulting from differences in surface finish is, in general, not great and in many cases the differences between average coefficients of friction for two or more finishes on a particular combination of metals are so small as to lack significance. Fine distinctions are therefore not warranted.

There are available for purposes of comparison 16 groups of tests in which all three directions of movement were tested with the same combinations of materials. Fourteen of these groups covered the three planed and milled finishes and two groups covered the rolled or planished finish.

For each material the three coefficients of friction corresponding to the three directions of movement were arranged in order of decreasing values of the coefficients of friction and grouped under each of the surface finishes considered. These data are shown in table 6.

The 14 groups of tests covering the 3 planed finishes and the milled finish were considered as a unit, the rolled or planished finish being considered alone.

For the 14 groups of tests, summations were then made of the total number of times each of the three directions of movement occurred in the high, intermediate, and low-value groups of the coefficient of friction for each combination of material and each surface finish shown in table 6. These totals were then converted into percentages of the total number of groups of tests. which resulted in the relations between the three directions of movement shown in table 7.

Table 6.—Effect of direction of movement on the magnitude of the coefficient of friction, for like metals in combination, unlubricated

	Coarse- planed finish		Medium- planed finish			planed		lled ish	Rolled or planished finish	
Materials used	Direction of movement	Coefficient of friction (k)	Direction of movement	Coefficient of friction (k)	Direction of movement	Coefficient of friction (k)	Direction of movement	Coefficient of friction (k)	Direction of movement	Coefficient of friction (k)
Bronze A	M ₂ M ₁ M ₂	10.390 .157 .150	M ₂ M ₃ M ₁	10. 161 . 151 . 138	M ₃ M ₁ M ₂	1 0. 154 . 152 . 143	M ₂ M ₃ M ₁	0. 162 1 . 154 . 148	M ₂ M ₁ M ₃	1 0. 16 . 15 1, 14
Bronze D	M ₂ M ₁ M ₃	1, 448 .163 .158	M ₂ M ₃ M ₁	1, 172 . 166 . 152	M ₁ M ₃ M ₃	1, 210 1, 204 1, 190	M ₂ M ₃ M ₁	. 146 . 146 . 140	M ₃ M ₁ M ₂	1, 19 . 17 1, 16
Rolled steel.	M ₁ M ₁ M ₃	1, 456 1, 224 1, 211			M ₁ M ₂ M ₃	1, 266 1, 243 1, 220	M ₁ M ₂ M ₃	1, 215 1, 176 1, 174		
Cast steel	M ₂ M ₃ M ₁	1, 392 1, 190 1, 174	*****		M ₁ M ₂ M ₃	1, 218 1, 198 1, 197	M ₁ M ₂ M ₂	1. 186 1. 162 1. 150		*****

¹ Seizure occurred

 \mathbf{M}_1 = Direction of movement and finish of plates parallel. \mathbf{M}_2 = Direction of finish of plates parallel, direction of movement normal to direction of movement normal to direction of the plates parallel and the pla M3=Direction of finish of plates at right angles.

It will be seen that 93 percent of the tests in which movement M2 was used fall within the groups of low and intermediate values of the coefficient of friction. while 79 percent of the tests in which movement M₂ was used fall within the groups of high and intermediate values of the coefficient of friction. Those tests in which movement M₁ was used are equally divided between the groups of low and intermediate and high and intermediate values of the coefficient of friction, being 64 percent in both cases.

Table 7.—Classification of values of coefficient of friction for the various directions of movement

Values of coefficient of friction (k)	Percentag direct	re of tests usi	ng each nent
	M_2	\mathbf{M}_1	\mathbf{M}_3
High Intermediate Low	Percent 57 22 21	Percent 36 28 36	Percent 5

Symbols used are: $M_1 = Direction$ of movement and finish of plates parallel. $M_2 = Direction$ of finish of plates parallel, direction of movement normal to direction of finish. $M_3 = Direction$ of finish of plates at right angles.

In the same 14 groups of tests seizure was noted as follows: For movement M_2 , 11 groups or 79 percent seized; for movement M_3 , 9 groups or 64 percent seized; for movement M₁, 7 groups or 50 percent seized. The combinations of like ferrous materials seized in all tests while the combinations of like bronzes seized in only 9 out of 24 tests or in 38 percent.

If the bronze and ferrous materials are considered separately, table 6 gives the following indications for bronzes:

For finish Pc movement M3 is best and movement M1 ranks second.

For finish P_M movement M₁ is best with movement M₃ ranking second.

For finish PF movement M2 is best with movements M₁ and M₃ rating equally for second place.

For finish M movement M, is best with movement M₃ second, with but slight differences between the two.

This tabulation shows, as has already been concluded from table 5, that for bronzes in combination the milled or medium-planed finishes give the lowest coefficients of friction. For these finishes, direction of movement M₁ is most satisfactory, although in general there is not a great difference between the coefficients for M1 and M3.

For ferrous materials, table 6 indicates that, considering all finishes, direction of movement M3 is superior to M_1 and M_2 , since it gives the lowest values in 4 out of 6 groups. However, in the case of the milled finish, the difference between M_3 and M_2 is not significant.

It is apparent from table 6 that, in the two groups of tests with rolled or planished finishes, direction of movement had no pronounced effect, as both high and low values of the coefficients of friction were evenly divided between movements M2 and M3 and seizure was noted in both the high and low groups. seizure was noted for movement M_1 .

If one finish and one direction of movement were to be selected for all combinations of metals, the one that would probably be most generally satisfactory would be the milled finish with the finishing cuts at right angles (M₃).

COMBINATIONS OF LIKE OR UNLIKE FERROUS MATERIALS HAD HIGHEST COEFFICIENTS OF FRICTION

In the 190 tests made, only 31 (exclusive of 2 tests with rusted cast iron) showed evidence of wear, the loss in thickness varying from 0.0005 to 0.0020 of an inch. Of the 31 tests showing wear, 22 were of like materials (10 bronzes and 12 ferrous materials) and 9 were of unlike materials (4 bronzes in combination with ferrous materials and 5 combinations of unlike ferrous

Table 8.—Effect of materials on the magnitude of the coefficient of friction (111 unlubricated sets considered)

		Group	no. 1—37 le	owest value	es of k 1	Group no	. 2—37 inte	rmediate v	values of k	Group	no. 3-37 h	ighest valu	ies of k
Combination of materials used	Number of sets tested	Number of sets	Percent- age of sets tested	Number of sets showing seizure	Number of sets showing wear	Number of sets	Percent- age of sets tested	Number of sets showing seizure	Number of sets showing wear	Number of sets	Percent- age of sets tested	Number of sets showing seizure	Number of sets showing wear
Bronze and ferrous	22	18	81. 8 71. 4		3	3	13. 6 28. 6		1	1	4.6		
Like ferrous	47 13 22	14	29.8	2	2	25 2 5	53. 2 15. 4 12. 7	8 2 5	4	8 11 17	17. 0 84. 6 77. 3	8 10 17	
Total	111	37		2	5	37		15	6	37		35	1

1 k = Coefficient of friction.

materials); 9 were lubricated and 22 were unlubricated. Twenty seized during testing and 11 did not seize.

In 20 cases wear was evident where a coarse-planed finish (P_C) was used, in 3 cases where a medium-planed finish (P_M) was used, in 5 cases where a fine-planed finish (P_F) was used, and in 3 cases where a milled finish (M) was used.

Wear occurred in 20 cases where the direction of movement and the directions of finish of both plates were parallel (M_1) , in 6 cases where the directions of finish were parallel and the direction of movement was normal thereto (M_2) , and in 5 cases where the directions of finish of the plates were at right angles (M_3) .

Seventeen of the combinations showing wear consisted of ferrous materials, 10 combinations consisted of bronzes, and 4 combinations consisted of bronze and ferrous materials. In three cases, where unequal wear occurred in the two plates of a combination of bronze and ferrous metal, the ferrous materials showed the greater wear.

In reaching any conclusion with respect to the importance of wear as disclosed by these tests, consideration should be given to the fact that the wear observed took place during only 1,200 slips of the test plates and that this number of movements represents only a very limited part of the total number to which bearing plates may be subjected during their useful Measurable wear occurred in only a small percentage of the total number of tests, and in the majority of the cases where it did occur, either a coarseplaned finish, which would not be recommended in any case, or a finish or direction of movement unsuited to the particular combinations of metals involved was used. Therefore, it seems probable that when a proper selection of materials and surface finishes is made, wear may be expected to be negligible.

Since the use of a lubricant appeared to be of doubtful value in permanently decreasing the coefficients for given materials, and furthermore, since tests of lubricated combinations were not made in all cases, only the 111 tests of unlubricated plates listed in table 3 (tests of rusted plates excluded) were considered in determining the relative merits of the materials tested for use in bridge bearing plates.

By arranging these 111 tests in the order of increasing coefficients of friction and dividing them into three groups of 37 tests each, the results shown in table 8 were obtained. These clearly indicate that combinations of bronze and ferrous materials and of unlike bronzes in combination are the most efficient, as 18 out of a total of 22, or 82 percent, and 5 out of 7, or 71 percent, respectively, of the total number of tests made

of these two classes of combinations fall within the group having the lowest coefficients of friction (group 1, table 8). Moreover, these two classes of combinations comprise 23 out of a total of 37, or 62 percent of the total tests falling in group 1.

In group 1, seizure was noted in only two combinations and was small in amount. These were like bronzes, both with a rolled finish, and seizure occurred in only 7 and 12 percent, respectively, of the total number of slips under any load intensity.

Group 3 of table 8 indicates that the combinations of unlike or of like ferrous materials are the most unsatisfactory of all of those tested, as 11 out of 13, or 85 percent, and 17 out of 22, or 77 percent, respectively, of the total number of tests made of these combinations fall within the group of the highest values of the coefficient of friction. These two classes of combinations comprise 28 out of 37, or 76 percent, of the tests falling within this group. Seizure was noted in all of the tests made of these two classes of combinations with the single exception of one combination of unlike ferrous materials.

It will be noted by reference to the general compilation of results (table 3) that the high lead bronzes in combination with like materials, or in combination with phosphor bronze or stainless steel, rank among the most satisfactory. The high lead bronze in combination with stainless steel shows next to the lowest coefficient of friction (0.110) of the 111 unlubricated combinations tested. The high lead bronzes in combination with like materials or in combination with phosphor bronze fall within the 13 lowest coefficients of friction of the 111 unlubricated combinations tested, with coefficients ranging from 0.128 to 0.132 as compared to the mean coefficient, 0.137, of group 1, table 3. This group comprises the 37 lowest coefficients of the 111 tests made of unlubricated plates.

EXPOSURE TO CALCIUM CHLORIDE HAD LITTLE EFFECT ON PLATES

Since the tests in this investigation indicated that combinations of ferrous materials and bronzes produced the lowest coefficients of friction and also indicated that rust may result in a substantial increase in the coefficient of friction, the use of stainless steel suggested itself because of its nonrusting properties. However, doubt existed as to the possible electrolytic action which might result from its use in combination with bronze when exposed to salt air. For the above reasons, a limited series of exposure tests was made in an attempt to obtain indications of electroyltic action, if such existed.

The procedure adopted was as follows: Eight samples of cast bronze, four of grade A and four of grade B,

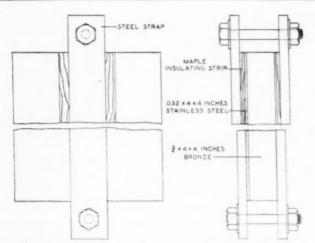


FIGURE 8.—ASSEMBLY OF PLATES FOR TESTS TO DETERMINE ELECTROLYTIC ACTION.

with machined surfaces, were used in combination with thin plates of stainless steel 0.032 inch thick with coldrolled surfaces as furnished by the manufacturer. These eight combinations of bronze and steel were clamped together by means of straps of iron or soft steel 1 inch wide bolted around the centers of the 4-inch square specimens used. In four sets of specimens the clamps were in direct contact with the specimens, thus forming a direct metallic or uninsulated bond between the two plates. In the other four sets of specimens thin strips of maple were placed between the clamps and specimens as insulation. The methods of clamping the specimens together and of insulating them are shown in figure 8.

One insulated and one uninsulated set of specimens were subjected to calcium chloride vapor by suspending them in the top of a brine tank of a cold storage plant. One insulated and one uninsulated set of specimens were subjected to a vapor of sodium chloride by suspending them over a saturated solution of this salt through which a small amount of air was continually passing, the top of the container being covered with canvas.

One set each of insulated and uninsulated specimens were immersed in saturated solutions both of calcium chloride and of sodium chloride. All specimens were left in place for 4 months. They were then removed, rinsed in hot water and dried with paper towels. All of the specimens were measured with micrometer calipers before and after exposure.

The four specimens exposed to calcium chloride either in vapor or immersed in the solution will be considered first (figs. 9 and 10). In no case was any apparent effect of exposure present on the contact faces of either the stainless steel or the bronzes. The outer face of the stainless steel immersed with no insulation between the specimens and the iron clamps showed a slight deposit of copper except where covered with the clamps. None of the other three stainless steel specimens showed any effect on the outer faces. Three of the four bronze specimens showed discoloration of the outer surfaces except where the surfaces were covered with either the clamps or the insulation strips. In no case was there any apparent breaking down of the surface or any

measurable change in thickness of either the bronze or steel specimens.

LIXPOSURE TO SODIUM CHLORIDE NOT DETRIMENTAL TO PLATES

In the case of the four specimens exposed to sodium chloride vapor or immersed in the solution, the following effects were noted (figs. 11 and 12).

The two steel specimens that were immersed showed no effect of immersion on the contact faces. The contact face of one bronze specimen showed no effect of immersion, while the other bronze specimen showed one small discolored spot where the contact between the steel and bronze was poor. One of the outer faces of the steel specimens showed no effect of immersion, while the other specimen was discolored in spots where salt crystals had formed. The outer faces of both bronze specimens were slightly discolored by immersion except where the surface was covered by the clamps or insulation strips.

The contact faces of both the two steel specimens and the two bronze specimens that were exposed to vapor showed discoloration in spots where contact between the steel and the bronze was poor. Both sets of specimens showed two bright spots on both the steel and the bronze where the contact between the bearing faces was good. The outer face of one steel specimen was discolored where it was in contact with the black iron clamps, while the other was discolored in two spots adjacent to the clamps. The outer faces of both bronze specimens exposed to vapor were discolored and one specimen showed two spots of corrosion adjacent to the iron clamps with a resulting increase in roughness of the surface.

No measurable change in thickness was found in any of the specimens and in only the one bronze specimen where corrosion was found was any apparent break-down of the surface noted. Figures 9 to 12 show both contact and outer faces after the exposure tests were completed. Differences in texture, color, and surface finish, with the resulting variations in the reflection of light, presented a difficult problem to the photographer. As a result, these photographs may give an exaggerated idea of the conditions of the various surfaces. However, they give a fair idea of the relative results of the various exposures.

Examination of these plates for evidences of electrolytic action revealed that only one of the eight sets of specimens gave indications of such action. When bronze A, in combination with stainless steel, was immersed in a solution of calcium chloride with no insulation between the iron clamps and the test specimens (i. e., with a direct metallic connection between the unlike materials), a deposit of copper was found on the outer surface of the steel except where it was covered by the clamp (fig. 9, no. 7). The outer surface of the bronze also showed an increase of copper on the surface

In none of the eight sets of specimens were effects of electrolysis evident on the contact faces of the specimens although in three of the bronze specimens and two of the steel specimens these faces were discolored in spots where contact between the two surfaces was imperfect. Due consideration should be given to the fact that the stainless steel plates used in these tests were only 0.032 inch thick and consequently were

FIGU

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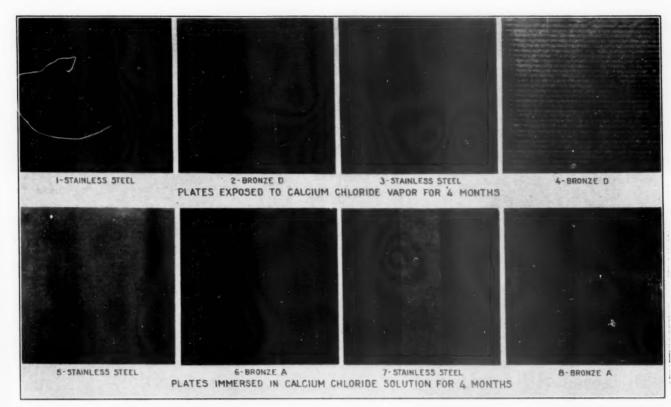


Figure 9.—Appearance of Bronze and Stainless Steel Bearing Plates After Immersion in and Exposure to Calcium Chloride. There Was No Insulation Between Clamps and Plates. Nos. 1, 2, 5, and 6 Were Contact Faces, and Nos. 3, 4, 7, and 8 Were Outer Faces of Plates.

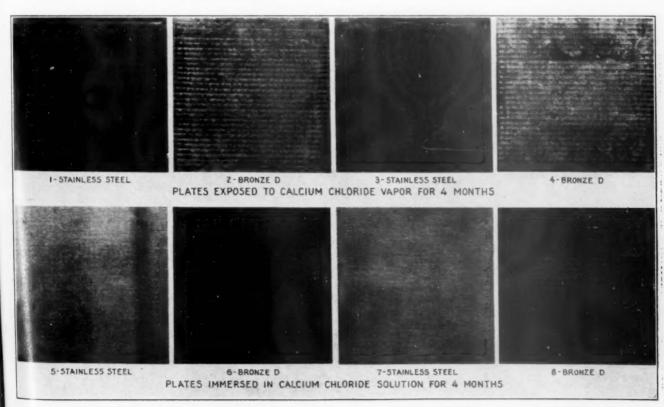


Figure 10.—Appearances of Bronze and Stainless Steel Bearing Plates After Immersion in and Exposure to Calcium Chloride. Strips of Wood Insulated the Iron Clamps From the Plates. Nos. 1, 2, 5, and 6 Were Contact Faces, and Nos. 3, 4, 7, and 8 Were Outer Faces of Plates.

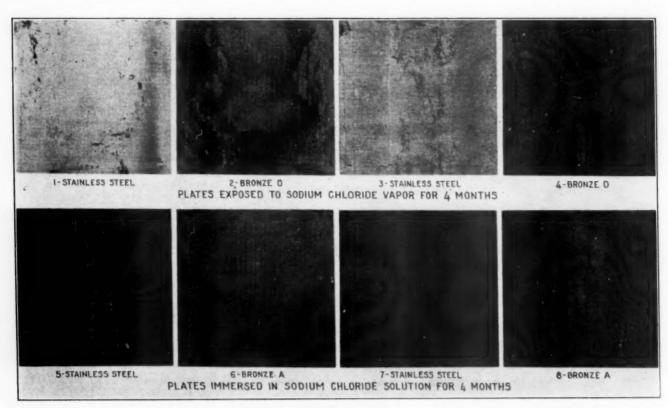


FIGURE 11.—APPEARANCES OF BRONZE AND STAINLESS STEEL BEARING PLATES AFTER IMMERSION IN AND EXPOSURE TO SODIUM CHLORIDE. THERE WAS NO INSULATION BETWEEN CLAMPS AND PLATES. Nos. 1, 2, 5, and 6 Were Contact Faces, and Nos. 3, 4, 7, and 8 Were Outer Faces of Plates.

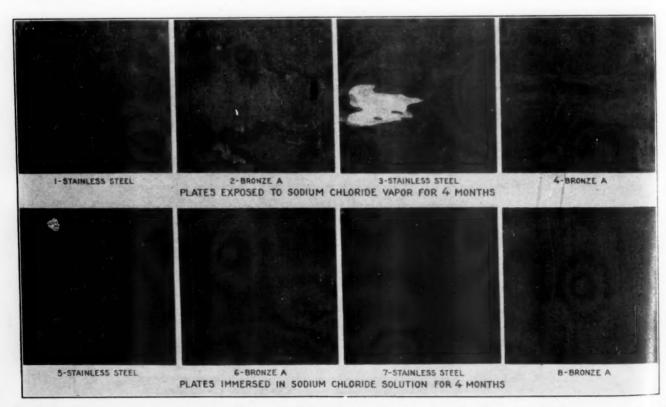


FIGURE 12.—Appearances of Bronze and Stainless Steel Bearing Plates After Immersion in and Exposure to Solium Chloride. Strips of Wood Insulated the Iron Clamps From the Plates. Nos. 1, 2, 5, and 6 Were Contact Fices, and Nos. 3, 4, 7, and 8 Were Outer Faces of Plates.

somewhat flexible. Moreover, they were clamped to the bronze specimens by clamps only 1 inch in width passing over the center of the specimens. As a result any slight unevenness, caused by shearing of the thinsteel plates or by marking with an identification number, caused faulty contact between the plates and allowed vapor or moisture to penetrate and settle. It is believed that, where thicker plates are used and are subjected to pressures usually existing on bridge bearing plates, contact between the surfaces will be such as to prevent penetration by either moisture or vapor. Four of the eight outer surfaces of the steel showed no effect, one showed the copper deposit mentioned above, and three were discolored in spots adjacent to the clamps undoubtedly resulting from the breaking down of the black iron of the clamps. No evidence of any break-down of the surface was apparent.

The outer surfaces of the bronze specimens showed the normal discoloration to be expected when finished metal is exposed to salt air, and in one specimen two small spots of corrosion with a slight increase in roughness were found adjacent to the iron clamps. The iron clamps all showed pitted and rusted surfaces as a result of exposure.

These tests would seem to indicate that for normal exposure to salt air no electrolytic action or breaking down of contact faces may be expected when bronze and stainless steel are used in combination if the contact between the plates is good.

CONCLUSIONS

- The coefficient of friction for bearing plates remains constant under varying loads for any combination of materials tested.
- 2. An initial application of graphite grease or other lubricant that will flow appears to be of doubtful value in permanently reducing the coefficients of friction when used under conditions such as obtained in these tests.

- 3. In general, for the materials tested the relative coefficients of friction, in increasing order of magnitude, are as follows:
 - a. Ferrous materials in combination with bronzes.
 - b. Hard bronzes in combination with softer bronzes.
 - c. Like bronzes in combination
- d. Ferrous materials in combination with like or unlike ferrous materials.
- e. Ferrous materials in combination where subject to rust.
- 4. The following are indicated as the most satisfactory finishes for various combinations of materials:
 - a. Ferrous materials in combination—a milled finish.
- b. Like bronzes in combination—a milled or medium-planed finish.
- c. Ferrous materials and bronzes in combination—a milled or fine-planed surface.
- d. A cold-rolled finish on bronze compares favorably with machined finishes provided the plates are rolled to a surface which will give uniform contact.
- 5. The directions of movement most satisfactory for machined plates are with finishing cuts at right angles (M₃) and with direction of movement and direction of finishing cuts parallel (M₁), with M₃ showing a slight superiority. With rolled or planished finishes, but slight variations in friction are caused by the direction of movement, although less seizure is noted when the direction of movement and the direction of finish are parallel.
- 6. Wear is probably a negligible factor when suitable materials and finishes are used.
- 7. The limited exposure tests made do not indicate that destructive corrosive action may be expected from the use of combinations of bronze and stainless steel when exposed to salt air.
- 8. If proper care is used in selecting materials and finishes, a coefficient of friction varying from 0.10 to 0.15 may be expected, with variations of 5 percent above and below mean values, for load intensities of the order of 250 to 1,000 pounds per square inch.

DISPOSITION OF STATE MOTOR-

[Compiled from reports

								For Stat	e highway p	urposes		
	Net total	Adjustments	Net total	Expenses of collec-	For other admin-	Construe-		Servic	e of State hig	hway oblig	ntions	
State	receipts of calendar year	due to undis- tributed bal- ances, etc. ¹	funds dis- tributed 3	tion and adminis- tration	istra- tive pur- poses 3	tion, main- tenance, and adminis- tration 4	State highway police	State highway bonds	State- assumed local obliga- tions [‡]	Notes and other short- term loans	Total	Total fo State highway purpose
labama	\$10, 313, 112	-\$3,068	\$10, 310, 044	\$29, 298	\$43,691	\$3, 735, 071	\$39,300	\$1 355 498			81, 355, 498	\$5, 129, 86
rizona	3, 278, 598		3, 278, 598	39, 946		1, 981, 576	82, 938	41,000,100	\$3, 059, 506		41,000, 200	2 064 51
rkansas	8, 261, 907	-15,798	8, 246, 109	304, 457	68, 118	1, 400, 390		2, 748, 773	\$3, 059, 506	\$70, 396	5, 878, 675	2, 064, 5 7, 279, 0
alifornia	39, 983, 955	-2,365,667	37, 618, 288	132, 687		24, 793, 382						24, 793, 3
oloradoonnecticut	6,009,533	-439	6, 009, 094	98, 134		4, 243, 132	73, 128					4, 316, 2
onnecticut	5, 671, 844	-159, 224	5, 512, 620	41,000		5, 471, 620						5, 471, 6
elaware	1, 481, 819	11 228, 563	1, 710, 382	6, 076		1, 049, 105	96, 621	52, 748	277, 269		330, 017	1, 475, 7
loridaeorgia	17, 896, 972 15, 771, 723	-10, 813	17, 886, 159	20, 427		7, 581, 351	58, 957		2, 552, 247		2, 552, 247	10, 192, 5
laho	3, 124, 297	-5, 325	15, 771, 723 3, 118, 972	472, 181 10, 292		7, 496, 569 2, 901, 555		007 105				7, 496, 5
linois	30, 385, 382	28, 714	30, 414, 096	142, 507	170 000	2, 901, 555 9, 566, 502		207, 125			207, 125	3, 108, 6
diana	19, 262, 319	20,114	19, 262, 319	81, 657	178, 002 67, 056	9, 391, 090	******				*******	9, 566, 5
wa	11, 549, 118	5,000	11, 554, 118	92, 118	07,000	3, 060, 253	********		3, 309, 747 693, 266		0 200 747	9, 391, 0
ansas	8, 961, 190	33, 289	8, 994, 479	295, 766	86,500	5, 356, 573	66 618		802 266		602 266	6, 370, 6
entucky	9, 835, 918	31, 398	9, 867, 316	48, 507	00,000	9, 794, 488	24, 321		093, 200		093, 200	9, 818,
entuckyouisiana	9 416 969	578, 665	9, 995, 634	62,000		0,104,400	20,020	8 064 450	693, 266		8, 064, 450	8, 064,
aine	4, 572, 827	-1,058	4, 571, 769	14, 872		2, 611, 947	148, 448	1, 253, 086	~~~~~~~~~		1, 253, 086	4, 013,
laryland	8, 278, 025		8, 278, 025	51, 331		2, 976, 166		1, 380, 548			1, 380, 548	4, 356,
fainefaryland	17, 334, 090	2, 824 -23, 476	17, 336, 914	50,000		3, 764, 015	200, 792	441, 930		15.445	457, 375	4, 422,
lichigan	22, 790, 561	-23,476	22, 767, 085	120, 945		12, 465, 565		4, 082, 060			4, 082, 060	16, 547, 6
finnesota	11, 362, 258	-35,584	11, 326, 674	166, 696		7, 267, 351	127, 937					7, 395, 3
fississippi	7, 512, 370	-3,242	7, 509, 128	26, 858	70,000	4, 268, 447	26, 349	**********				4, 294,
Iissouri	9, 845, 301	64, 699	9, 910, 000	49, 571	105, 585	5, 470, 283	139, 189	4, 145, 372			4, 145, 372	9, 754,
Iontana	3, 844, 542	78, 764	3, 923, 306	18, 631		3, 100, 035		804, 640			804, 640	3, 904,
Vebraska	9, 808, 734 962, 040	-7,028	9, 801, 706	95, 514		5, 370, 609						5, 370,
ew Hampshire	2, 868, 166	4 200	962, 040	1, 950		928, 972	16, 846		14, 272		14, 272	960,
lew Jersey	18, 205, 100	4, 360 18-1, 387, 702	2, 872, 526 16, 817, 400	4. 150 84. 959		1, 970, 753		726, 895			726, 895	2, 697,
Jew Mexico	2, 877, 605	1, 001, 102	2, 877, 605	62 325		475, 764 1, 301, 584		1, 597, 651			7, 597, 651	8, 073, 2, 815,
New Mexico New York 20	56, 311, 245	166, 865	56, 478, 110	92, 714		5, 024, 734	483, 436	3, 675, 900			1, 513, 696	2, 815,
orth Carolina	19, 147, 015	17, 533	19, 164, 548	6, 199	24, 995	5, 760, 418	179, 618	6, 602, 260	200 108		3, 675, 900 7, 001, 465	9, 184,
orth Dakota	2, 323, 387	-2,611	2, 320, 776	25, 000	24, 000	1, 523, 041	6, 959	0,002,209	399, 196		1,001,400	1, 530,
)hio	39, 169, 151	-1,354,539	37, 814, 612	183, 446		15, 654, 932	354, 386					16, 009,
klahoma	11, 877, 151	-324,787	11, 552, 364	237, 543			000,000					4, 911,
Pennsylvania	7, 942, 853	-99,525	7, 843, 328	26, 129		3, 649, 210	198, 473	2, 805, 233			2, 805, 233	6, 652,
ennsylvania	25 40, 651, 831	26 493, 817	41, 145, 648	209, 677		22, 723, 714	793, 531	3, 322, 949			3, 322, 949	26, 840,
Chode Island	2 106 204	58, 359	2, 164, 563	16, 973		1, 544, 353		301, 876	**********		301, 876	1, 846,
outh Carolina	25 8, 765, 749	-66,777	8, 698, 972	29 38, 500	20 9, 500	3, 522, 026			2, 524, 151	544	3, 642, 657	7, 164,
South Dakota	4, 315, 419	24, 079	4, 339, 498	44, 410		1, 877, 967						1,877,
Tennessee	14, 966, 016	234, 778	15, 200, 794	150, 594		2, 103, 571			2, 133, 833	4, 095, 377	6, 279, 566	8, 383,
		-86, 806	33, 519, 279	335, 345					8, 290, 061		8, 290, 061	24, 893,
Ttah	2, 714, 341 2, 048, 645	-29,341 $219,677$	2, 685, 000 2, 268, 322	8, 000 2, 200		2, 577, 183		449 447				2, 677,
Jirginia	13, 340, 505	-147, 169	13, 193, 336	164, 160	28, 885	1, 218, 366 6, 351, 567		447, 445			447, 445	1, 700.
Virginia Vashington Vest Virginia	12, 568, 379	-141, 109	12, 568, 379	22, 684	28, 880	4, 036, 904					476, 210	6, 827,
Vest Virginia.	6, 102, 941	-1,741	6, 101, 200	23, 468		1, 603, 958					97, 930 4, 233, 429	4, 134,
Visconsin	16, 249, 747	-825, 947	15, 423, 800	52, 421	178, 540	6, 286, 279			9 977 990		2, 277, 229	5, 836,
Wyoming	1, 931, 912	90, 403	2, 022, 315	11, 051	178, 340		32, 479	112,000	2, 211, 229		112, 000	8, 563,
Wyoming District of Colum- bia.	2, 197, 209		2, 572, 002	(36)							112,000	1, 414,
Total 37	619, 802, 062	-4, 221, 087	615, 580, 975	4, 275, 369	860, 872	258, 036, 693	3, 284, 703	57, 618, 031	25, 530, 777	4 181 769	87, 330, 570	348 651

¹ Amounts distributed during the calendar year differ in many cases from actual collections because of undistributed balances and lag between accounts of collecting agencies. Adjustments also include deduction of receipts not classed as highway-user imposts as follows: Proceeds of tax on gasoline used in aviation in Idaho, Maine, Michigan, Nebraska, Oregon, and Wyoming, and proceeds of tax on nonmotor-vehicle fuel in Ohio.

¹ In many States the proceeds of motor-fuel taxes, motor-vehicle fees, and motor-carrier taxes are placed in a common fund from which the distribution is made. In these cases the amounts distributed have been prorated in proportion to the receipts, not otherwise dedicated, from these three sources of revenue. See following tables.

¹ Where reported separately from collection expenses, funds allotted for motor-fuel inspection, administration of motor-vehicle department, and regulation of motor-vehicles are shown in this column.

¹ Includes funds allotted for expenditure on urban extensions of State highway system, where reported separately from other funds distributed for local roads and streets.

¹ County or local obligations assumed by State as reimbursement for local roads added to State system.

¹ In states indicated by star (*) law provides that allotments for work on local roads or streets may also be used for service of local highway obligations, but amounts so used not reported separately.

¹ In a number of States allotments for local road work may be used on city streets. This column shows allotments which were reported separately.

¹ To State general funds unless otherwise noted. Allocations to county or municipal general funds may have been used in part for highways, but such amounts not reported.

¹ For engineering expenses in connection with irrigation.

¹¹ For engineering expenses in connection with irrigation.

¹¹ For engineering expenses in connection with irrigation.

¹¹ For one engineering expenses in connection with irrigation.

¹¹ For one engineering expenses in connection

FUEL TAX RECEIPTS, 1935

of State authorities]

		rposes	nhighway pu	For nor				and streets 8	or local roads	F
State	Total	For other purposes	For education	For relief of unem- ployment or desti- tution	To general funds 8	For other highway purposes (park and forest roads, etc.)	Total	Service of local highway obliga- tions	For work on city streets?	For work on county and local roads
Alabama.							\$5, 107, 186			\$5, 107, 186
Arizona.	\$190,773	9 \$4, 106		\$186,667			983, 365			*983, 365
Arkansas.	,						594, 469	\$81,738	P100 101	512, 731
California.							12, 692, 219 1, 594, 700		\$182, 161	*12, 510, 058 10 1, 594, 700
Colorado.							1, 594, 700			1, 001, 100
	228, 563				11 \$228, 563	**********				******
Florida.	2, 568, 682	12 16, 434			2, 552, 248		5, 104, 495			0.502.010
Georgia.	5, 265, 960	1,789,808	\$2, 615, 477				2, 537, 013			2, 537, 013
Idaho. Illinois.	7, 361, 010			3, 512, 788	144.960		13, 166, 075		*6, 596, 832	*6, 569, 243
Indiana.	331, 426		0, 100, 900	0, 012, 100	331, 426		9, 391, 090		1, 878, 218	7, 512, 872
. Iowa.	000, 200						5, 092, 000			*5, 092, 000
Kansas.										2, 495, 756
Kentucky. Louisiana.	1, 869, 184	14 934, 592	934, 592					**********		
	1, 309, 134					**********	.543 416			543, 416
Maryland.	136, 687	15 123. 727		16 453, 789			3, 733, 293	642, 106	2, 312, 168	779, 019
Massachusetts.	9, 953, 789			16 453, 789	9, 500, 000	\$538, 204	3, 733, 293 2, 372, 739 6, 094, 185		*************	2, 372, 739 *6, 094, 185
	4, 330 67, 046				4, 330		3, 697, 644			*3, 697, 644
	07,040						3, 117, 474			*3, 117, 474
Missouri.								*********		****
							2 200 265		321, 180	*2, 901, 185
	1, 113, 218						3, 222, 365		321, 100	
New Hampshire.							170, 728	17 170, 728		
New Jersey.	5, 700, 585	19 404, 023	1, 332, 500	3, 964, 062			2, 958, 441	192, 763	• • • • • • • • • • • • • • • • • • • •	2, 765, 678
New Mexico.	20 110 222				21 39, 110, 555	********	8, 090, 771	******		*8, 090, 771
	39, 110, 555 1, 479, 326						4, 712, 527			22 4, 712, 527 765, 000
North Dakota	776				776		765, 000			765, 000
3 Ohio.	9, 487, 003		9, 487, 003				12, 134, 845		8 4, 929, 445	7, 205, 400 *2, 908, 983
8 Oklahoma.	3, 494, 006	24 3, 490, 778			3, 228	20, 280	2, 908, 983 1, 144, 003			*1, 144, 003
Oregon. Pennsylvania.	5, 124, 475	17 38, 206				46, 567	8, 924, 735		579, 361	*8, 345, 374
	301, 361	30, 200				10, 001				
South Carolina.	133, 605				29 133, 605		1, 352, 684			*1, 352, 684
South Dakota. Tennessee.	2, 356, 601 2, 434, 085	30 2, 242, 176 31 2, 329, 264		104, 821	114, 425	60, 520	4, 232, 978			4, 232, 978
Tennessee.	2, 434, 085 8, 290, 061	2, 329, 264					3, 434, 913			3, 202, 810
Utah.	0, 200, 001		0, 200, 001							*********
Vermont.							565, 751		***	565, 751
4 Virginia.	1,724	83 1, 724					6, 170, 790 7, 585, 574	84 79, 574	994, 320	32 6, 170, 790 6, 511, 680
	825, 287				************		241, 245	19, 3/4	904, 320	22 241, 245
8 Wisconsin.	2, 640, 898				33 2, 640, 898	109, 614	3, 878, 819		489, 436	3, 389, 383
Wyoming.	************						597, 207	**********	**********	597, 207
District of Columbia.						***********	2, 572, 002		2, 572, 002	
6 Total.37	110, 471, 016	11, 374, 838	26, 363, 586	15 549 969	67 194 220	775, 185	150, 546, 567	6, 271, 404	20, 855, 123	123, 420, 040

Pro-rata share service of highway relief bonds, a State obligation incurred for improvement of local roads.

Includes \$767, 240, pro-rata share of temporary loan to general fund for relief.

For service of institutional construction bonds, \$434,468; Department of Commerce and Navigation, \$90,000; less credit for excess allocations in 1934, (-) \$120,445.

Appropriations out of general fund for highway purposes have been credited against payments of motor-fuel tax and motor-vehicle fees to the State general fund and prorated in proportion to net receipts not otherwise dedicated.

To State general fund after crediting appropriations for highway purposes, \$37,614,987; New York City general fund, \$1,495,568.

For county roads under State control.

For service of general State debt.

Differs from total in a previous table issued by the Bureau—State motor-fuel tax receipts, 1935—by amount of refunds, \$57,009, reported subsequent to issuance of previous table. previous table.

In computing adjustment, amounts loaned to general fund for relief purposes in 1934 and 1935 (pro-rata share, \$3,622,384) have been included in the undistributed

balances.

17 For aircraft landing fields, \$25,824; cooperative work other departments, \$12,382.

28 Differs from total in a previous table issued by the Bureau—State motor-fuel tax receipts, 1935—by amount of inspection fees, \$181,605, reported subsequent to issuance of previous table.

28 Amount shown as payment to general fund represents proceeds of inspection fees paid to general revenue, \$181,605, less estimated cost of tax collection and inspection, as given above.

39 For payments on real-estate bonds.

30 Service of general fund bonds, \$2,116,489; Great Smoky Mountain Park bonds, \$211,649; aviation projects, \$1,126.

31 For county roads under State control in all but 3 counties, \$5,944,322; transferred to remaining 3 counties, \$225,468.

For a viation purposes.

Debt service charges on \$10,000,000 emergency relief bond issue prorated in proportion to allotments for State highways, local roads, and nonhighway purposes.

Includes \$500,000 to State general fund and \$2,140,898 to towns, cities, and villages in lieu of personal property tax formerly imposed on motor vehicles.

Paid out of general revenue. Amount not reported.

See notes 25 and 28.

DISPOSITION OF STATE MOTOR-

[Compiled from reports

								For State	e highway p	urposes		
	Net total	Adjustments	Net total	Expenses of collec-	For other	Construc-		Service	of State hig	hway obliga	ations	
State	receipts of calendar year ¹	due to undis- tributed bal- ances, etc. ⁸	funds dis- tributed 3	tion and adminis- tration 4		tion, main- tenance, and adminis- tration 8	State highway police	State highway bonds	State- assumed local obliga- tions ?	Notes and other short- term loans	Total	Total for State highway purposes
labama	\$3, 574, 151	-\$1,096	\$3, 573, 055	\$349,048		\$2,064,145	\$133,664	\$373, 015			\$373, 015	\$2, 570, 82
rizona	848, 146	-15, 266	832, 880	149, 466		654, 658	27, 400		**************************************	A00 005		682, 058
rkansas	2, 529, 191		2, 529, 191	75, 484		455, 460	86, 280	894, 005	\$995, 067	\$22, 895	1, 911, 967	2, 453, 70
alifornia	10, 562, 502 2, 206, 930	-613, 724	9, 948, 778 2, 206, 930	2, 028, 889 311, 620	\$36, 067	2, 931, 082	2, 068, 763				**********	4, 999, 84 72, 24
oloradoonnecticu	6, 108, 224		6, 108, 224	853, 699	\$30,007	72, 245 2, 754, 987	325, 000					3, 079, 98
Pelaware	1, 072, 079	14 332, 606	1, 404, 685	46, 654		728, 974	67, 138	36, 652	192, 661		229, 313	1, 025, 42
lorida	4, 954, 774		4, 954, 774	375, 204	174, 211	rao, er a	01,100	20,002				.,,
leorgia	1, 248, 278		1, 248, 278	165, 024	45, 577	754, 723						754, 72
daho	1, 880, 085	-84, 256	1, 795, 829	57,685		168, 325	53, 065					221, 39
llinois	20, 437, 737	318	20, 438, 055	941, 341	304, 279	7, 508, 748	893, 175	9, 081, 120	376, 789		9, 457, 909	17, 859, 83
ndiana	8, 154, 293	-53, 893	8, 100, 400	839, 447		3, 182, 090	385, 227					3, 567, 31
owa	10, 314, 046	-313, 374	10, 000, 672	752, 862		4, 442, 800	05 150		4, 805, 010		4, 805, 010	9, 247, 81
Cansas	3, 495, 576	-16, 027	3, 479, 549	255, 706	20 000	1, 994, 335	25, 159		261, 815		261, 815	2, 281, 30 2, 543, 88
Centuckyouisiana	3, 491, 413 3, 563, 380	-13, 823 -11, 66'	3, 477, 590 3, 551, 719	385, 599 145, 657	32, 099	2, 528, 753 2, 762, 785	15, 132 342, 477	300, 800			300, 800	3, 406, 06
Joine	3, 236, 078	-1,366	3, 234, 712	104, 556	12, 836	1, 786, 802	101, 552	857, 221			857, 221	2, 745, 57
Jarvland	4, 453, 440	-259, 198	4, 194, 242	246, 726	38, 403	1, 543, 461	260, 699				1, 140, 598	2, 944, 75
Maine Maryland Massachusetts	6, 305, 397	200, 100	6, 305, 397	1, 453, 460	35, 000	2, 328, 397	124, 208	273, 375			282, 930	2, 735, 53
Michigan	17, 601, 108	133, 288	17, 734, 396	1, 177, 833	00,000	2, 020, 001	250, 000	210,010		0,000	200,000	250, 00
Minnesota	7, 215, 403	250, 274	7, 465, 677	417, 663	361, 246	2, 469, 424	43, 472	2, 122, 000	1, 962, 820		4, 084, 820	6, 597, 71
dississippi	1, 740, 856	459	1,741,315	89, 309		181, 307	1, 157	***********				182, 46
Missouri	8, 311, 786		8, 311, 786	485, 415		4, 388, 842	111,672	3, 325, 857			3, 325, 857	7, 826, 37
Montana	1, 381, 568	-37,729	1, 343, 839	90, 967			72, 540	******				72, 54
Nebraska	1, 999, 405	8, 154	2, 007, 559	77, 421		575, 191	12, 500	********				587, 69
Nevada	263, 511	-17,496	246, 015	22, 163	********	153, 548	2,742	67, 562			67, 562	223, 85
New Hampshire	1, 691, 502	-4, 150	1, 687, 352	102, 943		1, 327, 734	136, 700	4, 953			4, 953	1, 469, 35
New Jersey	16, 623, 763	-13, 934	12, 007, 272 1, 103, 645	1, 109, 227 127, 564		2, 848, 883						2, 848, 8 439, 2
New Mexico New York 20	1, 117, 579 43, 956, 507	-280, 983	43, 675, 524	2, 345, 572	98, 071	439, 237 6, 919, 284	665, 714	5, 061, 880			5, 061, 880	12, 646, 87
North Carolina	6, 636, 748	632, 900	7, 269, 648	322, 043	30,011	2, 177, 914	67, 910	2, 496, 203	150, 929		2, 647, 132	4, 892, 93
North Carolina North Dakota	1, 422, 695	-156, 431	1, 266, 264	83, 905	24, 674	216, 343	20,000	a, 100, 200				236, 3
Ohio	21, 535, 578	127, 825	21, 663, 403	1, 321, 331		4, 815, 160	109,002					4, 924, 16
Oklahoma	3,861,366	-43,073	3, 818, 293	287, 156	256, 016	1, 284, 205			********			1, 284, 2
Oregon Pennsylvania	2, 748, 249	7, 345	2, 755, 594	318, 290		1, 137, 778	61,881	874, 636			874, 636	2, 074, 2
Pennsylvania	28, 758, 933	27-1, 782, 890	26, 976, 043	1, 391, 596	********	21, 137, 536	738, 140	3, 090, 998			3, 090, 998	24, 966, 67
Rhode Island	2, 900, 462	-1,494	2, 898, 968	259, 468		2, 269, 111						2, 269, 1
South Carolina	1,791,050	-12, 381	1, 778, 669	171, 748		736, 191	149, 265	221, 424	499, 933	108	721, 465	1, 606, 9
South Dakota		3, 991 -33, 989	1, 375, 017 3, 398, 328	71, 618 214, 089		264, 765 2, 751, 490	190, 922	66, 476			101, 964	264, 76 3, 044, 3
rennessee	15, 745, 897	-33, 989 -485	15, 745, 412	895, 557		4, 732, 671	308, 041	00, 470			101, 901	5, 040, 7
Utah	1, 070, 647	-233,382	837, 265	99, 765		2, 102, 011	000,011	737, 500			737, 500	737.5
Vermont	1, 377, 241	1, 208, 084	2, 585, 325	44, 491		1, 366, 064	38, 749	501, 686			501, 686	1, 906, 4
Virginia	5, 150, 755	9,741	5, 160, 496	312, 404		4, 479, 035	194, 960	173, 469			173, 469	4, 847, 4
Washington West Virginia	3, 495, 253		3, 495, 253	341, 161		2, 635, 070	507, 098					3, 142, 16
West Virginia	4, 820, 637		4, 820, 637	48, 459		1, 125, 795	29, 277	2, 973, 051			2, 973, 051	4, 128, 1
Wisconsin	10, 897, 032	-326,651	10, 570, 381	661, 541	35, 000	4, 199, 529			1, 538, 492		1, 538, 492	5, 738, 0
Wyoming District of Colum-	482, 893	-9,414	473, 479	9, 470		287, 351	10, 658	166, 000			166, 000	464, 0
District of Colum-	010 000		010.000	00 150	00 400							
bia	910, 226		910, 226	99, 172	63, 493	******						*****
Total	318, 747, 713	-6,239,672	312, 508, 041	22, 537, 468	1, 516, 972	113, 582, 228	8, 631, 339	34, 840, 481	10, 783, 516	68, 046	45, 692, 043	167, 905, 6

1 Amounts for many States differ from totals in a previous table issued by the Bureau—State motor-vehicle receipts, 1935—which gives receipts of the 1935 registration period.

2 Amounts distributed during the calendar year differ in many cases from actual collections because of undistributed balances and lag between accounts of collecting and expending agencies.

3 In many States the proceeds of motor-fuel taxes, motor-vehicle fees, and motor-carrier taxes are placed in a common fund from which the distribution is made. In these cases the amounts distributed have been prorated in proportion to the receipts, not otherwise dedicated, from these three sources of revenue. See tables that precede and follow this table.

4 Collection expenses in many States include service charges deducted by county and local collectors.

5 Where reported separately from collection expenses, funds allotted for collection of motor-fuel tax, payments to auto theft fund, and miscellaneous expenses of motor-vehicle regulation are shown in this column.

6 Includes funds allotted for expenditure on urban extensions of State highway system, where reported separately from other funds distributed for local roads and streets.

7 County or local obligations assumed by State as reimbursement for local roads and ded to State system.

4 In States indicated by star (*) law provides that allotments for work on local roads or streets may also be used for service of local highway obligations, but amounts so used not reported separately.

8 In a number of States allotments for local road work may be used on city streets. This column shows allotments which were reported separately. See note 6, 10 To State general funds unless otherwise noted. Allocations to county or municipal general funds may have been used in part for highways, but such amounts not reported.

11 To county and municipal general funds.

10 To State general natus tames where the reported.

11 To county and municipal general funds.

12 For engineering expenses in connection with irrigation.

13 Funds allotted to counties for use on both State and local roads.

14 For-rata share of State highway sinking fund transferred to general fund as a result of refunding operation which replaced sinking fund bonds with serial bonds.

15 For Confederate pensions and past-due teachers' salaries, \$190,755; prison camps, \$317.

VEHICLE RECEIPTS, 1935

of State authorities]

F	or local roads	and streets				For no	nhighway pu	urposes		
For work on county and local roads *	For work on city streets	Service of local highway obliga- tions	Total	For other highway purposes (park and forest roads, etc.)	To general funds 10	For relief of unem- ployment or desti- tution	For education	For other purposes	Total	State :
*********								12 \$1, 356	\$653, 183 1, 356	Alabama. Arizona.
*********								***********		Arkansas.
*\$2, 920, 044			\$2, 920, 044							California.
13 802, 721			802, 721		730, 476	\$253, 801			984, 277	Colorado.
2, 174, 538			2, 174, 538		14 220 604		*********			Connecticut.
					14 332, 606		\$4 405 950		332, 606	Delaware.
			-*		91, 882		\$4, 405, 359	15 191, 072	4, 405, 359	Florida.
*1, 516, 754			1, 516, 754		31,002			- 191, 0/2	282, 954	Georgia. Idaho.
1, 187, 635			1, 187, 635		144, 968				144, 968	Illinois.
1, 272, 836	\$318, 209		1, 591, 045		2, 102, 591				2, 102, 591	Indiana.
			******							Iowa.
942, 534			942, 534							Kansas.
516, 007			516, 007						*********	Kentucky.
371, 745			281 846							Louisiana.
311, 143	637, 894		371, 745 637, 894		*******	326, 461			200 401	Maine.
1, 467, 761	901, 001		1, 467, 761	\$332,930	**********	326, 461 16 280, 711			326, 461 280, 711	Maryland. Massachusetts.
*15, 959, 812			15, 959, 812	\$332, 930	346, 751	~ 280, /11			346, 751	Massachusetts. Michigan.
		**********			89, 052			***************************************	89, 052	Minnesota.
*1, 469, 542			1, 469, 542						00, 002	Mississippi.
										Missouri.
1, 151, 818	28, 514		1, 180, 332						******	Montana.
1, 342, 447			1, 342, 447							Nebraska.
		17 \$115, 022	115, 022							Nevada.
6, 894, 896		1, 154, 266	8, 049, 162							New Hampshire.
146, 412		1, 104, 200	146, 412		19 390, 432				390, 432	New Jersey. New Mexico.
*9, 168, 706			9, 168, 706		11 19, 416, 297				19, 416, 297	New York,20
22 1, 781, 725			1, 781, 725						272, 924	North Carolina.
16, 342			16, 342					23 905, 000	905, 000	North Dakota.
14 °15, 178, 280	(15)		15, 178, 280					20 239, 630	239, 630	Ohio.
*1, 990, 916 *356, 686			1, 990, 916							Oklahoma,
300, 080	538, 919		356, 686 538, 919	6, 323				14 05 FDO	05 500	Oregon.
	000, 818		338, 919	43, 316				out our	35, 538 370, 389	Pennsylvania. Rhode Island.
						310, 389			370, 389	South Carolina.
1, 030, 101			1, 030, 101	8, 533						South Dakota.
				0,000		138, 376		29 1, 487	139, 863	Tennessee.
*9, 809, 143			9, 809, 143							Texas.
694 000										Utah.
634, 335			634, 335							Vermont.
11, 924			11, 924					29 628	628	Virginia.
22 641, 663			641, 663		10 2, 392				2, 392	Washingon. West Virginia.
2, 277, 770	328, 915		2, 606, 685	90, 386	31 1, 438, 748				1, 438, 748	West Virginia. Wisconsin.
			aj 000, 000	50, 000	1, 100, 110				1, 100, 190	Wyoming.
					88 747, 561			1-0000-000	747, 561	District of Columbia.
00 000	-	-	-	-		-				
83, 035, 093	1, 852, 451	1, 269, 288	86, 156, 832	481, 488	26, 759, 863	1, 369, 738	4, 405, 359	1, 374, 711	33, 909, 671	Total.

16 Pro-rata share (approximate) of debt service on nonhighway portion of Emergency Public Works loan.
17 Pro-rata share service of highway relief bonds, a State obligation incurred for improvement of local roads.
18 Includes \$4,594,247, pro-rata share of temporary loan to general fund for relief.
19 To State general fund, \$146,412; to county general funds, \$244,020.
20 Appropriations out of general fund for highway purposes have been credited against payments of motor-fuel tax and motor-vehicle fees to the State general fund and corrated in proportion to net receipts not otherwise dedicated.
10 To State general fund after crediting appropriations for highway purposes, \$15,213,905; New York City general fund, \$4,202,392.
19 For county roads under State control.
10 To real estate bond and interest fund, \$900,000; Bureau of Criminal Identification, \$5,000.
10 General law provides that this allotment shall be used for highway purposes. It is provided, however, that during 1933, 1934, and 1935 amounts shall be paid to counties did townships for other than highway purposes, equal to amounts which would have been produced by the 1930 levies on personal property for other than highway purposes.
18 Allotments to municipalities not reported.
19 Allotments to municipalities not reported separately for 1935.
19 For hospitalization of indigent persons injured in motor-vehicle accidents.
10 In computing adjustment, amounts loaned to general fund for relief purposes in 1934 and 1935 (pro-rata share, \$3,717,186) have been included in the undistributed lances.

20 For algerett lending 804de \$24,000 general fund for relief purposes in 1934 and 1935 (pro-rata share, \$3,717,186) have been included in the undistributed lances.

18 In computing adjustment, amounts loaned to general the departments, \$11,517.

28 For aircraft landing fields, \$24,021; cooperative work other departments, \$11,517.

29 For aviation purposes.

30 To cities.

31 To towns, cities, and villages in lieu of personal property tax formerly imposed on motor vehicles.

32 To District of Columbia general fund.

DISPOSITION OF STATE MOTOR-

[Compiled from reports

							For Sta	te highway	purposes		
	Net total	Adjustments due to un-	Net total	Expenses of col-	Construc-		Servic	e of State hi	ghway oblig	ations	
State	receipts of calendar year	distributed balances, etc. ¹	funds dis- tributed ²	lection and adminis- tration	tion, mainte- nance, and adminis- tration ³	State highway police	State highway bonds	State assumed local obliga- tions 4	Notes and other short- term loans	Total	Total for State highway purposes
Alabama	\$109, 592 122, 394	-\$14,335 -3,246	\$95, 257 119, 148	\$23, 142 10, 653	\$54, 749 103, 930	\$4,350					\$54, 749 108, 280
Arkansas California Colorado	2, 038 2, 014, 661 294, 473	661, 925 -33, 942	2, 038 2, 676, 586 260, 531	380, 038 40, 432	392 276, 818 141, 314				\$20		2, 038 736, 818 141, 314
Connecticut Delaware	167, 974	-16, 059	151, 915		48, 540						48, 540
FloridaGeorgia	221, 216 298, 705 77, 231	-37, 694 -28, 845	221, 216 261, 011 48, 386	47, 227 133, 475 20, 480	93, 996	27, 906				*********	93, 996 27, 906
IllinoisIndiana	(13) 513, 783	-267, 921	245, 862	69, 774	176, 088						176, 088
Iowa Kansas Kentucky Louisiana	269, 984	-9, 449 1, 730 -80, 050	421, 970 869, 722 189, 934	112, 936 227, 583 74, 985 1, 142	346, 647 114, 664	88, 863 285		44, 919			
Maine	20, 288		1, 142 20, 288	20, 288						*********	
Maryland	(14) 64, 815 387, 171	-298, 939	64, 815 88, 232	37, 127 87, 152						**********	
Minnesota Mississippi Missouri	100, 250	230 4, 946 40, 082	19, 028 95, 304 487, 691	19, 028 1, 300 64, 893	217, 353					164, 710	387, 593
Montana Nebraska	22, 164	-3, 695	18, 469	18, 469							
Nevada New Hampshire	192, 310		192, 310 2, 821	8, 553 2, 821	180, 532	3, 225	*********			**********	183, 757
New Jersey New Mexico New York	84, 253	15 -28, 292 -3, 397	55, 961 83, 604	11, 400	18, 564 59, 470	12, 734		**********			18, 564 72, 204
North Carolina North Dakota	132, 687	-28, 936	132, 687 23, 437	23, 437	41, 595	1, 297	47, 673	2, 882			93, 447
OhioOklahoma	727, 874 796, 776	-19, 349	727, 874 777, 427	155, 240 37, 126	439, 881 740, 301	9, 958	********				449, 839 740, 301
Oregon Pennsylvania Rhode Island	7, 635 14, 976	32, 485 17—430	784, 662 7, 205 14, 976	100, 380	316, 787 5, 119	22, 902 178	243, 522 746			746	583, 211 6, 043
South Carolina	87, 882 312, 435	-3, 499 66, 413 20, 608	84, 383 378, 848 286, 145	16, 347 28, 200	60, 761 339, 701 135, 269	*********	**********				\$ 60, 761 339, 701
TexasUtah	267, 412	-700	63, 886 268, 820	62, 341 54, 404 31, 439	9, 482 228, 530	8, 851					140, 282 9, 482 237, 381
Vermont	138, 460		138, 460 186, 126	19, 914 186, 126	92, 049						92, 049
West Virginia	59, 632 1, 429, 481	-15, 446	59, 632 1, 414, 035	404, 364	15, 729		41, 536				57, 26
Wyoming District of Columbia	138, 268		138, 268 166, 982	23, 271	112, 356	2, 641					114, 997
Total	12, 421, 383	-74, 289	12, 347, 094	2, 570, 463	4, 370, 617	188, 720	962, 224	48, 658	1, 765	1, 012, 647	5, 571, 98

Amounts distributed during the calendar year differ in many cases from actual collections because of undistributed balances and lag between accounts of collecting and expending agencies.

In many States the proceeds of motor-fuel taxes, motor-vehicle fees, and motor-carrier taxes are placed in a common fund from which the distribution is made. In these cases the amounts distributed have been prorated in proportion to the receipts, not otherwise dedicated, from these 3 sources of revenue. See preceding tables.

Includes funds allotted for expenditure on urban extensions of State-highway system, where reported separately from other funds distributed for local roads and streets.

County or local obligations assumed by State as reimbursement for local roads added to State system.

In States indicated by star (*) law provides that allotments for work on local roads or streets may also be used for service of local highway obligations, but amounts so used not reported separately.

To State general funds unless otherwise noted. Allocations to county or municipal general funds may have been used in part for highways, but such amounts not reported.

For engineering expenses in connection with irrigation.

CARRIER TAX RECEIPTS, 1935

of State authorities]

F	or local roads	and streets				For no	nhighway pu	rposes		
For work on county and local roads	For work on city streets	Service of local highway obligations	Total	For other highway purposes (park and forest roads, etc.)	To general funds 6	For relief of unem- ployment or desti- tution	For education	For other purposes	Total	State
\$17, 366			\$17,366							Alabama.
			***********	********				7 \$215	\$215	Arizona. Arkansas.
					\$1, 268, 170			8 14, 340	1, 282, 510	California. Colorado.
				**********	10 103, 375	*********			103, 375	Connecticut. Delaware.
306		\$161,535	161, 535 306		10 8, 256 10, 792			12 22, 442	12, 454 33, 234	Florida. Georgia.
**********										Idaho. Illinois.
*309, 034			309, 034		~~~~	*****				Indiana. Iowa.
161, 710			161,710		***********					Kansas.
								*********		Kentucky. Louisiana.
				******						Maine.
					27, 688			***********	27, 688	Maryland. Massachusetts.
					1,080				1,080	Michigan.
*93, 229			93, 229		775	*********			775	Minnesota. Mississippi.
35, 205			35, 205			*******		******		Missouri.
		**********	***********							Montana. Nebraska.
										Nevada.
29, 876			37, 397					******		New Hampshire. New Jersey. New Mexico.
										New York. '
18 34, 028		100000000000	34, 028						5, 212	North Carolina. North Dakota.
122, 795			122, 795							Ohio. Oklahoma.
*99, 311			99, 311	1,760						Oregon.
	130		130				-		1,032	Pennsylvania. Rhode Island.
					18 7, 275				7, 275	South Carolina.
				10, 947	76, 646	6, 803		19 73	83, 522	South Dakota. Tennessee.
										Texas. Utah.
										Vermont.
									26, 497	Virginia. Washington.
16 2, 367			2, 367						1, 009, 671	West Virginia. Wisconsin.
					10 166, 982					Wyoming. District of Columbia.
					-	-				
1, 261, 232	130	169, 056	1, 430, 418	12, 707	2, 713, 451	6, 800	4, 198	37, 070	2, 761, 522	Total.

For service of county and city bonds.
Funds allotted to counties for use on both State and local roads.
Funds allotted to counties for use on both State and local roads.
Funds allotted to counties for use on both State and local roads.
Funds allotted to counties for use on both State and local roads.
Funds allotted to counties on motor carriers reported.
Funds allotted to confederate pensions and past-due teachers' salaries, \$22,405; for prison camps, \$37.
Receipts from weight tax on motor carriers, \$5,154, included in motor-vehicle receipts, preceding table.
Adjustment includes \$29,937, pro-rata share of temporary loan to general fund for relief purposes.
For county roads under State control.

DISPOSITION OF RECEIPTS FROM STATE

[Compiled from reports

							For Sta	te highway	purposes		
	Net total receipts of	Adjustments due to un-	Net total	Expenses of col- lection	Construc-		Servic	e of State hi	ghway oblig	ations	
State	calendar year ¹	distributed balances, etc. ¹	funds dis- tributed	and adminis-	tion, mainte- nance, and adminis- tration 4	State highway police	State highway bonds	State- assumed local obliga- tions !	Notes and other short- term loans	Total	Total for State highwa purpose
abama	\$13, 996, 855	-\$18,499	\$13, 978, 356	\$445, 179	\$5, 853, 965		\$1, 728, 513			\$1, 728, 513	\$7, 755, 4
rizona	4, 249, 138	-18,512	4, 230, 626	200, 065	2, 740, 164	114, 688			***********	# #00 000	2, 854, 8
kansas	10, 793, 136	-15, 798	10, 777, 338	448, 059	1, 856, 242	86, 280	3, 643, 547	\$4,055,430	\$93, 311	7, 792, 288 460, 000	9, 734, 30, 530,
difornia	52, 561, 118 8, 510, 936	-2, 317, 466 -34, 381	50, 243, 652 8, 476, 555	2, 541, 614 486, 253	28, 001, 282 4, 456, 691	2, 068, 763 73, 128	460,000				4, 529,
nnecticut	11, 948, 042	-175, 283	11, 772, 759	894, 699	8, 275, 147	325, 000					8, 600,
laware	2, 553, 898	14 561, 169	3, 115, 067	52, 730	1, 778, 079	163, 759	89, 400	469.930	1	559, 330	2, 501,
orida	23, 072, 962	-10,813	23, 062, 149	617, 069	7, 581, 351	58, 957		2, 552, 247		2, 552, 247	10, 192,
orgia	17, 318, 706	-37,694	17, 281, 012	816, 257	8, 345, 288						8, 345,
aho	5, 081, 613	-118,426	4, 963, 187	88, 457	3, 069, 880	80, 971	207, 125			207, 125	3, 357
nois	50, 823, 119	29, 032	50, 852, 151	1, 566, 129	17, 075, 250	893, 175	9, 081, 120	376, 789		9, 457, 909	27, 426
diana	27, 930, 395	-321, 814	27, 608, 581	1, 057, 934	12, 749, 268	385, 227		0 114 727		8, 114, 757	13, 134 15, 617
va	22, 294, 583 13, 324, 758	-317, 823 18, 992	21, 976, 760 13, 343, 750	957, 916 865, 555	7, 503, 053 7, 697, 555	180, 640		8, 114, 757		1, 000, 000	8, 878
nsasntucky	13, 597, 315	-62, 475	13, 534, 840	541, 190	12, 437, 905	39, 738		1, 000, 000		1,000,000	12, 477
uisiana	12, 981, 491	567, 004	13, 548, 495	208, 799	2, 762, 785	342, 477	8, 365, 250			8, 365, 250	11, 470
aine	7, 829, 193	-2, 424	7, 826, 769	152, 552	4, 398, 749	250, 000	2, 110, 307			2, 110, 307	6, 759
aryland	12, 731, 465	-259, 198	12, 472, 267	336, 460	4, 519, 627	260, 699	2, 521, 146			2, 521, 146	7, 301
assachusetts	23, 704, 302	2,824	23, 707, 126	1, 575, 587	6, 092, 412	325, 000	715 305		25,000	740, 305	7, 157
ichigan	40, 778, 840	-189, 127	40, 589, 713	1, 385, 930	12, 465, 565	250, 000	4, 082, 060			4, 082, 060	16, 797
innesota	18, 596, 459	214, 920	18, 811, 379	964, 633	9, 736, 775	171, 409	2, 122, 000	1, 962, 820		4, 084, 820	13, 993
ississippi	9, 353, 476	-7, 729	9, 345, 747	187, 467	4, 449, 754	27, 506	B 005 000			7 cor 000	4, 477
issouri	18, 604, 696	104, 781	18, 709, 477	705, 464	10, 076, 478 3, 100, 035	256, 391	7, 635, 939			7, 635, 939	17, 968 3, 977
ontanaebraska	5, 248, 274 11, 808, 139	37, 340 1, 126	5, 285, 614 11, 809, 265	128, 967 172, 935	5, 945, 800	72, 540 12, 500	804, 640				5, 958
evede	1, 417, 861	-17,496	1, 400, 365	32, 666	1, 263, 052	22, 813	67, 562	14 979		81, 834	1, 367
evadaew Hampshire	4, 562, 489	210	4, 562, 699	109, 914	3, 298, 487	136, 700	731, 848	14, 212		731, 848	4, 167
ew Jersey	34, 913, 118	22-6, 032, 485	28, 880, 633	1, 194, 186	3, 343, 211	130, 100	7, 597, 651			7, 597, 651	10, 940
ew Mexico	4, 082, 185	-17, 331	4, 064, 854	201, 289	1, 800, 291	12, 734	1, 513, 696				3, 326
ew York 25	100, 267, 752	-114, 118	100, 153, 634	2, 536, 357	11, 944, 018	1, 149, 150	8, 737, 780			8, 737, 780	21, 830
orth Carolina	95 016 450	650, 433	26, 566, 883	353, 237	7, 979, 927	248, 825	9, 146, 145	553, 007		9, 699, 152	17, 92
orth Dakota	3, 798, 455	-187,978	3, 610, 477	157, 016	1, 739, 384	26, 959					1, 766
h10	61, 432, 603	-1, 226, 714	60, 205, 889	1, 660, 017	20, 909, 973	473, 346					21, 38
klahoma		-387, 209 -59, 695	16, 148, 084 11, 383, 584	817, 841 444, 799	6, 936, 338 5, 103, 775	000 050	3, 923, 391				6, 936
regonennsylvania	69, 418, 399		68, 128, 896	1, 601, 273	43, 866, 369	283, 256 1, 531, 849	6, 414, 693				51, 81
hode Island	5, 021, 642	56, 865	5, 078, 507	291, 417	3, 813, 464	1, 001, 010	301, 876			301, 876	4, 11
hode Islandouth Carolina	10, 644, 681	-82, 657	10, 562, 024	236, 095	4. 318, 978	149, 265	1, 339, 386	3, 024, 084	652	4, 364, 122	8, 833
outh Dakota	5, 998, 880	94, 483		144, 228	2, 482, 433					.,,	2, 48
ennessee	18, 663, 870	221, 397	18, 885, 267	427, 024	4, 990, 330	190, 922	120, 100	2, 133, 833	4, 132, 610	6, 386, 543	11, 56
exas		-87, 991	49, 328, 577	1, 285, 306	21, 345, 965	308, 041		8, 290, 061		8, 290, 061	29, 94
tah		-261,315		139, 204	2, 805, 713	108, 668	737, 500				3, 65
ermont		1, 427, 761	4, 853, 647	46, 691	2, 584, 430	73, 309	949, 131				3, 600
irginia	18, 629, 720	-137, 428		525, 363	10, 922, 651	194, 960	649, 679				11, 76
Vashington Vest Virginia	16, 249, 758 10, 983, 210		16, 249, 758	549, 971 71, 927	6, 671, 974 2, 744, 582	507, 098 29, 277	40 97, 930 7, 248, 016			97, 930 7, 248, 016	7, 27
Visconsin	28, 576, 260			1, 331, 866	10, 485, 808	29, 211	7, 248, 010	3 815 791		3, 815, 721	14, 30
Vyoming	2, 553, 073			43, 792	1, 669, 285	45, 778	278,000	0,010,721		278, 000	1, 993
Vyoming District of Columbia	3, 274, 417			162, 665	1,009,200	70,110	210,000			210,000	1,00
Total	950, 971, 158	-10,535,048	940, 436, 110	21 761 344	275 090 538	19 104 769	93, 420, 736	38 389 051	4 951 573	134, 035, 260	599 190

Includes receipts from (1) motor-fuel taxes, (2) motor-vehicle fees and fines, and (3) special imposts on motor vehicles operated for hire (motor-carrier taxes). See preceding tables, which give distribution of these three classes of receipts separately.

Amounts distributed during the calendar year differ in many cases from actual collections because of undistributed balances and lag between accounts of collecting and expending agencies. Adjustments also include deduction of receipts not classed as highway-user imposts as follows: Proceeds of tax on gasoline used in aviation in Idaho, Maine, Michigan, Nebraska, Oregon, and Wyoming, and proceeds of tax on nonmotor-vehicle fuel in Ohio.

Includes expenses of collection and administration of motor-fuel tax, motor-vehicle fees, and motor-carrier taxes, and miscellaneous expenses of motor-vehicle regulation.

tion.

Includes funds allotted for expenditure on urban extensions of State highway system, where reported separately from other funds distributed for local roads and

Includes funds allotted for expenditure on those extensions of state algorithms.

County or local obligations assumed by State as reimbursement for local roads added to State system.

In States indicated by star (*) law provides that allotments for work on local roads or streets may also be used for service of local highway obligations, but amounts so used not reported separately.

In a number of States allotments for local road work may be used on city streets. This column shows allotments which were reported separately. See note 4.

To State general funds unless otherwise noted. Allocations to county or municipal general funds may have been used in part for highways, but such amounts referenced. * To State general funds unless otherwise noted. Allocations to county or municipal general runds may have been used in part to reported.

* To county and municipal general funds.

16 For engineering expenses in connection with irrigation.

17 For service of county and city bonds.

18 Funds allotted to counties for use on both State and local roads.

19 Funds allotted to counties for use on both State and local roads.

19 State highway sinking fund transferred to general fund as a result of refunding operation which replaced sinking-fund bonds with serial bonds.

19 Includes \$8,266 to cities and towns.

10 To Division of Airways, \$16,616; Dade Memorial Park, \$818.

10 For Confederate pensions and past-due teachers' salaries, \$2,000,000; prison camps, \$3,322.

10 To ports of New Orieans and Lake Charles Harbor for harbor improvement.

10 To Conservation Department for oyster propagation, \$75,000; Chesapeake Bay ferry companies, \$48,727.

20 Debt service on nonhighway portion of emergency Public Works loan.

21 Service of highway relief bonds, a State obligation incurred for improvement of local roads.

IMPOSTS ON HIGHWAY USERS, 1935

of State authorities]

F	or local roads	and streets				For no	nhighway p	urposes		
For work on county and local roads	For work on city streets ?	Service of local highway obligations	Total	For other highway purposes (park and forest roads, etc.)	To general funds ⁸	For relief of unem- ployment or desti- tution	For Education	For other purposes	Total	State
\$5, 124, 552			\$5, 124, 552		9 \$653, 183				\$653, 183	Alabama.
*983, 365 512, 731	**********	\$81,738	983, 365 594, 469			\$186,667		10 \$5, 677	192, 344	Arizona.
*15, 707, 322	\$182, 161	401,100	15, 889, 483		1, 268, 170			11 14, 340	1 000 510	Arkansas.
12 2, 476, 206	\$100, 101		2, 476, 206					11 14, 340	1, 282, 510 984, 277	California. Colorado.
2, 174, 538			2, 174, 538		13 103, 375				103, 375	Connecticut.
					19 061, 169				561, 169	Delaware.
9 897 210		5, 266, 030	5, 266, 030		13 2, 560, 504		\$4, 409, 557	16 16, 434	6, 986, 495	Florida.
2, 537, 319 *1, 516, 754	***********	*********	2, 537, 319 1, 516, 754		963, 349		2, 615, 477	17 2, 003, 322	5, 582, 148	Georgia.
*7, 756, 878	*6, 596, 832		1, 516, 754		289, 237	3, 512, 788	2 702 002		7 808 070	Idaho.
8, 785, 708	2, 196, 427		10, 982, 135		2, 434, 017	3, 312, 788	3, 703, 953		7, 505, 978 2, 434, 017	Illinois. Indiana.
*5, 401, 034			5, 401, 034		2, 101, 011				2, 434, 017	Indiana. Iowa.
3, 600, 000		*********	3,600,000							Kansas.
516, 007	***********		516, 007							Kentucky.
915, 161			012 101					19 934, 592	1, 869, 184	Louisiana.
779, 019	2, 950, 062	642, 106	915, 161 4, 371, 187		12, 960	208 461		10 100 707	400 140	Maine.
3, 840, 500	2, 900, 002		3, 840, 500	\$871, 134		20 734 500		19 123, 727	463, 148 10, 262, 188	Maryland.
*22, 653, 997			22, 053, 997	0011, 101	352, 161				352, 161	Massachusetts. Michigan.
*3, 697, 644			3, 697, 644		156, 098				156, 098	Minnesota.
*4, 680, 245			4, 680, 245		775				775	Mississippi.
35, 205 1, 151, 818	00 514		35, 205			1				Missouri.
1, 151, 818 *4, 243, 632	28, 514 321, 180		1, 180, 332							Montana.
4, 245, 032	321, 180		4, 564, 812			1, 113, 218			1, 113, 218	Nebraska.
		21 285, 750	285, 750	*********						Nevada. New Hampshire.
9, 690, 450			11, 045, 000			3, 964, 062	1, 332, 500	23 404, 023	5, 700, 585	New Hampshire. New Jersey.
146, 412			146 412		34 390, 432			404, 020	390, 432	New Mexico.
*17, 259, 477			17, 259, 477		30 58, 526, 852				58, 526, 852	New York 35.
27 6, 528, 280			6, 528, 280		1, 757, 462				1, 757, 462	North Carolina.
781, 342 *22, 506, 475	10 4, 929, 445		781, 342 27, 435, 920				0 407 600	25 905, 000	905, 776	North Dakota.
*4, 899, 899	4, 929, 145		4, 899, 899		3, 228			31 239, 630 31 2 400 778	9, 726, 633	Ohio.
*1, 600, 000			1, 600, 000	28, 363	3, 220			22 3, 490, 778	3, 494, 006	Oklahoma. Oregon.
*8, 345, 374	1, 118, 410		9, 463, 784	89, 883	1,032	5, 086, 269		34 73, 744	5, 161, 045	Pennsylvania.
********						671, 750		- 10, 138	671, 750	Rhode Island.
*1, 352, 684	***************************************		1, 352, 684		35 140, 880				140, 880	South Carolina.
1, 030, 101 4, 232, 978			1, 030, 101	80, 000	114, 425	286 000		36 2, 242, 176 37 2, 330, 824	2, 356, 601	South Dakota.
9, 809, 143			4, 232, 978 9, 809, 143			250, 000			2, 657, 470	Tennessee.
0, 000, 143			9, 009, 143				8, 290, 061		8, 290, 061	Texas.
1, 200, 086			1, 200, 086							Utah. Vermont.
3º 6, 170, 790	************		6, 170, 790					³⁹ 2, 352	28, 849	Virginia.
*6, 523, 604	994, 320	40 79, 574	7, 597, 498			1 825, 287		⁸⁾ 2, 352	825, 287	Washington.
27 885, 275	010 011	*********	885, 275	000 000	41 2, 392				2, 392	West Virginia.
5, 667, 153 597, 207	818, 351		6, 485, 504 597, 207	200, 000	43 5, 089, 317				5, 089, 317	Wisconsin.
381, 201	2, 572, 002		2, 572, 002	**********	43 914, 543				014 540	Wyoming.
	2, 012, 002		2, 012, 002		2014, 043	********			914, 543	District of Columbia.
207, 716, 365	22, 707, 704	7, 709, 748	238, 133, 817	1, 269, 380	86, 657, 644		30, 773, 143	1	147, 142, 209	Total.

Includes \$5,391,424 temporary loan to general fund for relief.

For service of institutional construction bonds, \$434,468; Department of Commerce and Navigation, \$90,000, less credit for excess allocations in 1934, (-) \$120,445.

Appropriations cut of general fund for highway purposes have been credited against payments of motor-fuel tax and motor-vehicle fees to the State general fund properties in proportion to met receipts not otherwise dedicated.

To State general fund after crediting appropriations for highway purposes, \$52,828,892; New York City general fund, \$5,697,960.

To real estate bond and interest fund, \$900,000; Bureau of Criminal Identification, \$5,000.

Allotment from motor-fuel tax only. Municipal allotments to general funds. Amounts so used not reported separately.

Allotment from motor-fuel tax only. Municipal allotments from motor-vehicle fees not reported separately in 1935.

For service of general State debt.

In computing adjustment, amounts loaned to general fund for relief purposes in 1934 and 1935, \$7,340,000, have been included in the undistributed balances.

For aircraft landing fields, \$49, 845; cooperative work, other departments, \$23,899.

To State general fund, \$133,605; to counties and cities, \$7,275.

For ayments on real-estate bonds.

Service of general-fund bonds, \$2,116,489; Great Smoky Mountain Park bonds, \$211,649; aviation projects, \$2,686.

For aviation purposes.

For aviation purposes.

6 Debt service charges on \$10,000,000 emergency relief bond issue prorated in proportion to allotments for State highways, local roads, and nonhighway purposes.

17 Oction 18 Debt service charges on \$10,000,000 emergency relief bond issue prorated in proportion to allotments for State highways, local roads, and nonhighway purposes. 4 To Clues. \$1,509,671 to State general fund and \$3,579,646 to towns, cities, and villages in lieu of personal-property tax formerly imposed on motor vehicles. To District of Columbia general fund

STATUS OF FEDERAL-AID HIGHWAY PROJECTS

1936 -1937

AS OF NOVEMBER 30, 1936

			COMPLETED		25	UNDER CONSTRUCTION		APPROV	APPROVED FOR CONSTRUCTION	NO	BALANCE O
STATE	APPORTIONMENT	Letimated Total Cost	Federal Aid	Miles	Estimated Total Cost	Federal AM	Miles	Entimated Total Cost	Foderal Aid	Miles	ABLE FOR NEW PROJECTS
Alabama Ariaona Arianasa	3,564,709	\$ 51,600	\$ 25,800	98.3	\$ 710,181 1,019,637	\$ 355.090 807.3 ⁴ 3	20.1	\$ 730,700 254,800 1,765,401	179,220	75.3	\$ 4,462,047 1,199,944 2,511,190
Contraction of the contraction o	9.508.671	3.259.773	1.884.211	0.80	9.341.966	5.348.228	246.7	2,778,299	1,599,878	60.3	
Colorado	4,575,14	2,914,634	1,543,884	109.8	3,277,034	1,804.071	118.7	1,280,437	166.511	50.7	
Connecticut	1,582,913	491,873	245.937	9.5	727,093	361.344	6.9	120,600	60.240	30	
Delaware	1,218,750	305,920	152,960	30.3	339,069	164,048	6.0	436,402	204,962	2 6	
Georgia	6.336.443	936.738	416.776	72.1	2.435.848	1.217.904	128.7	921,133	450.951	39.0	
Idaho	3,065,304	1,927,993	1,145,730	235.2	1,450,283	867.845	73.8	1,06,340	243,151	25.6	
Illinois	10,325,922	5.190.075	2,589,322	90.5	6.858.774	3,394,913	25.9	3.657.650	1,983,610	80,80	2,358,078
lows	6,466,628	6.757.971	3,196,508	15.5	3,342,843	1,621,270	トカー	2,090,518	1,010,224	0.49	1
Kansas	6,631,085	2.903.124	1,500,886	599.0	4,629,975	2,288,486	357.5	2,212,052	1,106,010	114.7	
	1.557.930	1,463,437	780.1050	200	1.204.776	609.174	41.1	591.690	296.845	13.1	1
Maine	2.177.197	1,904,831	951,618	58.7	799,888	399.944	18.5	295,120 ROL RVR	147,560	10.9	
Massachusetts	3,465,364	333.935	166,968	3.1	4.490,403	2,195,201	17.5	14,206	7,102		
Michigan	7,668,768	5,517,385	2.754.470	224.5	8,371,468	4,185,734	225.2	1,204,594	740 040	35.5	117,26
Visalesinei	4.387.636	100.819.1	31/18131	24.3	294.105	147.052	16.3	1.133.470	567.035	70.9	3.673.54
Missouri	7,601,800	3,456,539	1.724,004	W22.8	6.537,120	3,267,422	241.3	2.529,454	1,390,349	119.2	1,219,42
NOT CHANGE	5,122,333	1,760.971	2,105,635	384.1	2.697.817	1.510.508	172.3	649.237	325,316	29.2	1,180,87
Nebraska Nevada New Hampshire	3,189,479	1,448,617	754.643	269 269 269 269 269	2,801,922 691,420	594.663	2.4	009.00	30,855	4. 10.10.	1,337,039
James Tanasana	3.352.469	1.833.713	916.817	28.1	2.680.249	1.262.810	26.1	324,309	162,155	5.4	1.010.64
New Mexico	3,990,023	5.571,651	1.623.798	116.2	1,935,274	1,196,066	171.2	908,535	552.567	33.1	617,59
North Caroline	5,879,466	1,989,822	050, 466	254.2	2.705.079	1,325,591	247.6	1,905,773	883,086	16.1	2,676,73
Ohio	9,131,204	1.474.536	737.268	56.9	6.717.210	3,183,286	71.2	587,960	292,480	5.8	4.918.17
Oklahoma	5,884,927	2,153,021	1,122,895	76.9	1,714,378	898,650	60.3	1,113,320	529,529	43.1	3,333,85
Oregon Pennsylvania	10.695,448	5.289.095	P. 644, 102	80.9	7.762.600	1.871.166	8.5	2.735.688	1.355.849	37.8	2.822.131
Shode Island	1,218,750	23,810	11,905	.3	593.768	296,884	9.9	486,757	243,379	a.	666,582
South Carolina South Dakota	3,381,337	32,682	15,000	188.7	3.235.070	1,309,620	239.1	1,818,052	718,750	124.8	1,337,967
Tennesses	5,268,270	1.915.051	955.394	80.3	857,474	426,732	33.0	302,878	151,439	10.0	3.732.701
Texas	5,548.821	9,281,213	4,629,891	526.8	5,658,953	2,825,805	264.3	2,668,582	1,330,044	167.0	6,763,081
Vermont	1,218,750	1.323.336	659.042	6.39	763,404	354.753	20.5	129,620	64,750	4.3	140,205
Virginia Washington	4,559,200	2,157,864	1.076.576	# 0 # 0	2,144,464	1.383.771	187.9	1.954.728	205,100	200	200
West Virginia Wisconsin	6,090,504	398,060	1,755.618	150.3	1,134,980	1,975,646	36.1	779,046	389,523	17.3	1,560,728
Wyoming	3,121,972	2,780,220	1,696,458	347.3	1,179,293	730,843	145.0	152,790	\$.100	30.8	600,571
District of Columbia Hawaii	1,218,750				1467,855	191,167	6.2	69,938	张心去	1.6	952,829
TOTALS	ohs seo oon	an. sos 411				10 0/0 000	1	or cal sal.			and Cale and

CURRENT STATUS OF UNITED STATES WORKS PROGRAM HIGHWAY PROJECTS

(AS PROVIDED BY THE EMERGENCY RELIEF APPROPRIATION ACT OF 1935)

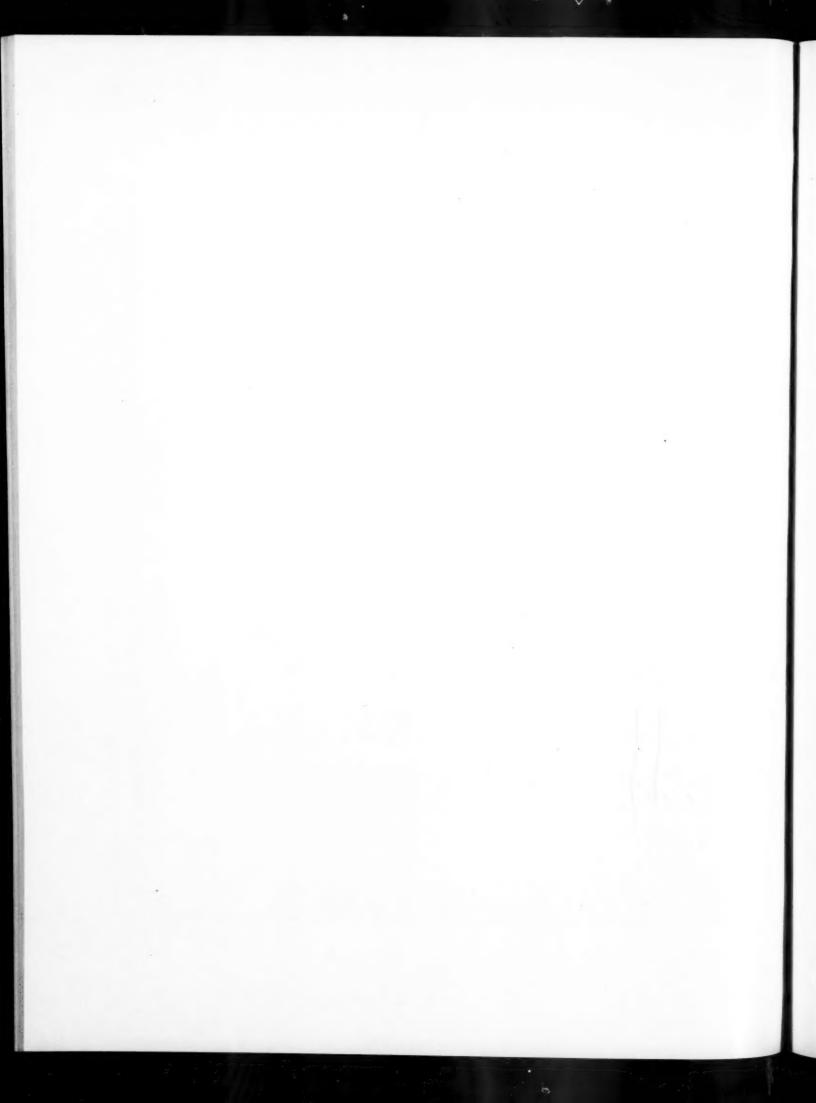
AS OF NOVEMBER 30, 1936

date 4 may			COMPLETED		UNI	UNDER CONSTRUCTION		APPROV	APPROVED FOR CONSTRUCTION	NO	BALANCE OF
SINIE	ATORIBONARNI	Estimated Total Cost	Works Program Funds	Miles	Estimated Total Cost	Works Program	Miles	Estimated Total Cost	Works Program Fundo	Miles	ARLE FOR NEW PROJECTS
Mehama	# 4,151,115	151.426	\$ 954,131	0.0	\$ 3,050,432	\$ 3.050,432	78.5	\$ 68,086	\$ 68,086	8.7	\$ 78,465
Arkansas	3,352,061	2,150,928	2,133,168	208.9	1,126,473	1,124,671	138.2	55,329	55,221	11.9	39.001
California	7.747.928	4,804,519	4,623,801	197.3	2,998,628	2,975,468	26.7	69.672	69,672	1.2	78,987
Connecticut	3,395,263	1,892,021	1,885,276	93.1	239,486	581.031	0.0	204.306	294.306	6.8	1,270,518
belaware	900,310	183,996	180,518	33.3	575.071	467,1425	29.5	106,430	106,420	4.0	145,946
Florida	2,597,144	769.624	769,624	34.45	1,712,444	1,712.44	64.3	70,781	70,781	at 0	163, 44
Idebo	2,222,747	1.739.499	1.692.671	145.6	510,235	010,000	37.7	21,660	21,660	25.4	17,876
Illinois	8,694,009	6,488,432	609.454.9	357.8	2,005,885	2,005,885	96.7	219,610	219,610	16.6	13,905
ndiane	4,941,255	1,235,967	1,232,664	59.7	3,828,728	3,608,823	168.8	37,924	37.924	6.3	61.843
Kanass	4,991,904	1.979,584	2,043,503	306.4	3,076,433	3.015.184	163.8	12.0	18,200	0.	1,5/6
Kentucky	3,726,271	1,732,303	1,724,277	236.1	1,424,606	1,424,606	105.6	355,705.	195,696	8,1	221,691
Louisiana	8,890,429	939,645	602,230	53.5	1,851,075	1,654,642	104.8	335,053	275,018	16.4	158,539
Maryland	1,676,799	1,171,746	1,170,514	10.9	405,523	623,523	13.05	84,600	502,954	7.5	16,161
Massachusetta	3,262,885	17.71	\$2.21	1.1	2,034,905	2,034,905	16.6	856.377	503.016	1.	607,210
Michigan	6,301,414	5,156,800	5.096.270	244.3	1,046,421	1,046,421	43.6	203,200	158,200	20 u	523
ilasiasirmi	3,457,552	1,530,341	1.526.274	116.7	1.555.771	1.554.402	5000	315.059	315,059	27.1	61.817
Missouri	6,012,652	3.251.055	3,219,982	685.8	2,405,820	2,289,863	90.5	602,777	435,632	1.7	67.175
Montaba	3,676,416	3.261.295	3,260,529	184.7	371.674	363.704	10.6				52.083
Nebraska	3.870.739	1,956,679	1,922,319	202.5	1,579,504	1,578,000	155.2	118,068	118,066	12.2	252,333
New Hampshire	945,225	847.194	476,066	24.3	260.796	250,723	0.00	89.423	87,975		130.461
ew Jersey	3,129,805	571.768	571,769	13.2	2,287,721	2,271,566	15.9	207,045	198,076	4.7	88,394
New Mexico New York	2,871,397	2,037,358 6,148,781	2,036,654 5,869,919	156.7	h 976, 518	1 848 720	36.2	156.277	156,277	10°0	73,148
orth Carolina	4,720,173	1,282,143	1,282,143	85.0	3,069,133	3,036,544	182.7	300,671	234,131	19.4	167.355
North Dakota	2,867,245	1,202,146	1,200,622	182.7	1,298,432	1,294,997	122.9	154.511	154.511	20.5	217,115
OID	7,670,815	2.233.273	2.210.463	18,1	4,278,746	4,156,035	147.7	1,085,310	1,068,105	65.5	236,212
Oklaboma	3.038.642	1.960.160	1,907,126	12/12	1.964.628	1.50K.17	10 m	600.009	600000	40.0	332,587
Pennsylvania	9.347,797	1,296,303	1.234,644	67.4	1,953,278	1,949,240	57.9	2,117,071	2,116,182	69.5	4,047,731
Rhode Island	989,208	730,630	720,034	15.4	259,501	259,501	3.5	9,673	9.673		
South Dakota	2.976.454	1.627.862	1.627.862	2000	897,926	897.926	100.1	207.147	254,009	19.01	322,678
Tennesses	4,192,460	1,558,721	1.554.796	71.8	1,496,888	1,496,888	51.9	506,607	506,607	18.4	634,169
Texas	11,989,350	9,515,614	8,624,872	868.5	3,534,481	3,230,556	243.4	188.047	89,975	10.0	43,948
Vermont	924,306	784,678	687.532	90	237,731	193,455	3.0	33,020	19,910	O. at	23.410
Virginia	3,652,667	2,502,384	2,526,123	829.8	767,689	767.509	180.9	189.806	189,806	31.8	169,230
Visutinia	2,231,412	194,382	194.382	11.8	1.801.289	1.797.745	67.9	128.465	127.732	10.3	111.551
Wisconsin	4,823,884	4,600,425	4,135,575	309.5	907.340	678.123	31.5	2.030	2.030	6.0	8,156
W yourne	2,219,155	1,340,450	1,340,443	109.0	859,398	840,528	31.1				38,184
District of Columbia Hawaii	926,033	243.307	228,809	1,0	401,855	395.297	6.4	54,482	53.884	1.5	248,044
0 14 1000	100 000 000	. con and . Can					-				

CURRENT STATUS OF UNITED STATES WORKS PROGRAM GRADE CROSSING PROJECTS

			COMPLETED					UNDER CONSTRUCTION	TION		-	APPR	APPROVED FOR CONSTRUCTION	LUCTION			
				Z	NUMBER				Z	NUMBER					NUMBER		BALANCE OF
STATE	APPORTIONMENT	Estimated Total Cost	Works Program Funds	Consider Township Township Township Township	4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	111111	Estimated Total Cost	Works Program Funds		13312		Estimated Total Cost	Works Progress Funds			1][1][1	FUNDS AVAIL ABLE FOR NEW FROJECTS
Alabama	\$ 4,034,617	\$ 606,753	\$ 606.753			#	\$ 2,961,384	\$ 2,961,384	36			8 313.0k7	\$ 313,047	~		80	# 153.43
Arkansas	3.574.060	1,135,951	1,131,634		4		1,726,085	1,723,087	22	-		662,597	545, 199	100	-	89	57.79
California Colorado Connecticut	7,486,362	1,076,063	1,055,063	20	9		4,467,380 868,611 563,087	4,329,593 868,583 491,009	25	oı	-	म्।०'म्हम्	410,464	-	Q		316,426 707,921 727,661
Delaware Florida Georgia	415,239 2,827,883 4,895,949	660,331	658,600	2-	#		143,486	1,430,789	- 2-9	N		456,292	1456.292	17			298,23 282,200
Idaho Illinois Indiana	1,674,479	824,073 2,423,431 497,831	821,481 2,422,894 497,831	25.	-		5.528.177	5.528.177	10 W R	5=		2,139,800	2,139,800	-=	O.	8 9	374,874
Iowa Kansas Kentucky	5,600,679	1.507.566	1,460,776	300	<i>a</i> -	-	3,568,132	3,531,469	123	- c		691,074 46,736	574,020	= ~-	-	10 m	माम्भूद
Louisiana Maine Maryland	3,213,467	493.350	493,016	2	-		1,447,148 584,695	1,447,148 584,103	ე <u>ച</u> ∞ ಇ	u - r		966,512	922.046	80 - P	m a	Ng	844,272 268,066 547,699
Massachusetts Michigan Minnesota	6,765,197	2.231.975	2.231.975	295	a w	39	2,634,481	2.634,481 4.509.797 2.891.610	202	EEN	po*	382,770	382,770	, cu	-	-	23,429
Mississippi Missouri Montana	3,241,475	308,981	308,961	80 W	n 0		2,331,184 5,695,929 403,583	5,499,685	200		-	56,000	36,000	#-		ma	646,786
Nebraska Nevada New Hampshire	3,556,441	370.830	370.830	55	- 0		531,025	1,588,885	200		5 -	3.630	3.630	2	-	8 80	92,147
New Jersey New Mexico New York	3,983,826	59.838	59.838	00			865.128	2,467,743 865,127	- w=			163,319	163,319	- cs	0.1		1,292,927
North Carolina North Dakota Ohio	4,823,958 3,207,473 8,439,897	579.548	579,548	68	10	-	1,765,711	2.257.073	28	one		1,108,520	1,108,520	100	e - a	19	586,681
Oklaboma Oregon Pennsylvania	5,004,711 2,334,204 11,483,613	1,208,387 562,923 390,192	1,208,387 562,923	26	- m	1	1,918,749 1,804,273 6,341,869	1,918,749	8 0 M	m mi	- 0	385,124	385,124	9	OJ PO	-	1,492,450
Rhodé Island South Carolina South Dakota	699,691 3,059,956 3,249,086	398,464 441,975 568,566	398,464	2 = 7	- 0 -	200	277,805 1,416,102 1,508,246	276.739 1,405,024 1,508,246	26	- w a	01	218,406	218,356	r.		17	24,468 1,002,253 846,619
Tennessee Texas Utah	3,903,979	2.739.062	2.739,082	94-	w	9	6,915,308	6,908,931		25	2	563,646 765,488 93,695	563.646 765,487 93.695	0 ma		130	1,531,235
Vermont Virginia Washington	3,774,287	461,762 853,786 868,175	182,923	153	N mm	2	1,343,569	1,304,569	- 10.00	- ~ 10	0	551,960	34.745	w 0		v= 0	1,134.537
West Virginia Wisconsia Wyoming	5,082,683	1.661.704	1,661,704	12.4	CV.		1,225,701 2,785,641 863,106	2,720,560	- 92	tr. 10		493.227 536,470	493.227	10		a	959.033
Dist. of Columbia Hawaii	410,804						425.564 522.380	396.804	20								14,000
TOTATE	200 000 300	22 502 600		- 12	-	H										-	





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Report of the Chief of the Bureau of Public Roads, 1934. 10 cents.

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An Economic and Statistical Analysis of Highway-Construction Expenditures. 15 cents.

Highway Bond Calculations. 10 cents.

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SEPARATE REPRINT FROM THE YEARBOOK

No. 1036Y . . Road Work on Farm Outlets Needs Skill and Right Equipment.

TRANSPORTATION SURVEY REPORTS

Report of a Survey of Transportation on the State Highway System of Ohio (1927).

Report of a Survey of Transportation on the State Highways of Vermont (1927).

Report of a Survey of Transportation on the State Highways of New Hampshire (1927).

Report of a Plan of Highway Improvement in the Regional Area of Cleveland, Ohio (1928).

Report of a Survey of Transportation on the State Highways of Pennsylvania (1928).

Report of a Survey of Traffic on the Federal-Aid Highway Systems of Eleven Western States (1930).

A complete list of the publications of the Bureau of Public Roads, classified according to subject and including the more important articles in Public Roads, may be obtained upon request addressed to the U. S. Bureau of Public Roads, Willard Building, Washington, D. C.

CURRENT STATUS OF UNITED STATES PUBLIC WORKS ROAD CONSTRUCTION

AS PROVIDED BY SECTION 204 OF THE NATIONAL INDUSTRIAL RECOVERY ACT (1934 FUNDS) AND BY THE ACT OF JUNE 18, 1934 (1935 FUNDS)

AS OF NOVEMBER 30, 1936

	APPORTIC	APPORTIONMENTS		COMPLETED	TED			UNDER CONSTRUCTION	RUCTION		APPROVED	APPROVED FOR CONSTRUCTION	NOLL	FOR NEW	FOR NEW PROJECTS
STATE	Sec. 204 of the Act of June 16, 1933 (1934 Fund)	Act of June 18, 1934 (1935 Fund)	Total Cost	1934 Public Works Fundo	1935 Public Works Funds	Mileage	Estimated Total Cost	1934 Public Works Funds	1935 Public Works Funds	Mileage	1934 Public Works Funds	Public Works Funds	Mileage	1934 Public Works	Public Works Funds
Alabama Arizona	\$8,370,133 5,211,960	2,641,935	815,386,528	\$ 6,304,382 5,204,512 6,613,093	\$ 3.584.390 2.605.036 3.320.347	760.1 542.9 619.3	\$ 394,771 12,500 143,231	\$ 52,665	\$ 339,310 12,500 72,991	15.8	\$ 31,389	\$ 309,252	10.9	8 13,085 7,448 13,834	\$ 26.890 24.399 27.511
Arkansas California Colorado	15,607,354	7.932,206	30,579,892	15,582,063	7,769,804 3,441,857	539.0	115,026	59,618	6,619	-		820		3,849	46,567 37,530 141,924
Connecticut Delaware Florida	1,619,088 5,231,854	2,661,343	2,680,794 8,897,748 13,210,656	1,818,604 5,175,534 9,317,893	2.344.564 3.168,476	128.3	109,467	689,804	105,524 230,665 667,832	6.18 6.19	% .300 84,072	67.339	50.00	280,531	2,682
Idaho Illinois	1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1	2.277.486 8.921,401 5.088.963	7,024,481	4,416,568 16,893,752 9,896,355	2,185,517 7,817,218 4,733,207	500.5 706.4 474.1	1,789,642	594,209	52.034 1,068,172 244,553	15.8	37.300	7,100	12.8	8,910 45,509 12,405	38,049 28,911 52,475
Iowa Kansas Kentucky	10,055,660 10,089,604 1,517,359	5,118,361	15,454,949	10,054,900	4,996,568 3,571,867	1.222.2	340,073 126,993 275,154	59,003	321,000 61,887 214,500	1.5.	8,569	23,250		261 4 1,649	59,120
Louisiana Maine Mandand	5,828,591	2,963,932	8,982,708 5,244,109 5,536,045	5,731,008	2.592.759	193.5	318,465	56.549	198,436	13.4		26,540	2.50	41,034 8.038 87,489	8.737 8.737 352.376
Massachusetts Michigan	6,597,100	3,350,474	9,869,513	6,552,734	2,659,290 6,264,495 4,745,392	766.9	168.750	40,113 56,110	420,416 47,600 376,135	200		136.788	-3.9	84.036	178.524 3.685 269,224
Mississippi Missouri Montana	6.978.675	3.540.227	12,693,004	6.735,410	2,992,646 4,720,320 3,701,189	721.4	653.726 2.176.630 56,546	188,861	1,334,260 56.546	15.1	3,960	41,503	1.9	50.445 71.949 14.272	57,061
Nebraska Nevada New Hammahire	7,828,961	3,964,364	12,828,547	7,813,593	3.604.469	1,018.3	262,047		274,622 25,006 4,174	27.8		1,650	5.9	15,368	7,111
New Jersey New Mexico	6,346,039	3,220,879 2,941,700	8,255,287 8,788,982 38,763,582	6,046,046 5,734,176 21,778,431	1.607.061 2.827.536 10.094.963	743.9	1.964.004	315,051	1,409,346 107,130 982,899	14.1	133,947	99.275	1.3	97.330 58.759 17.913	105.197
North Carolina North Dakota	5,522.293 5,804,448	2,938,967	14,891,750 8,367,434 8,406,155	9,159,957 5,509,008	2,025,925 2,025,164 7,212,293	1.342.1 2.094.0 784.7	365.770	291,910	73.860	2.63	\$1.017 15.703 .34,023	200,573 101,140 87,539	17.0	19,408 65,418 24,114	60.583 461,789 47.549
Oklahoma. Oregon	9,216,798	3.097,814	14,535,440 9,882,293 28,714,652	9,146,565 6,039,064 18,496,822	8.303.265 2.923.060 8.746.721	804.9 467.6 1.050.6	182,756 95,469 516,605	67,007 11,308 96,463	377.896	6.00	153,388	174,301	N 10	3,226	91.865 63.352 307.948
Rhode Island South Carolina South Dakota	5,459,165	1,014,572	3,144,150 7,914,944 9,222,498	1,998.708 5,239.171 5,816.751	1,012,094 2,379,367 2,829,595	614.7	336.927	158,946	139.753	34.7	46,320	37.133	23.8	14.728 93,248	105,293
Tennemee	8,492,619 24,244,024 4,194,708	12,302,991	13,431,633	83,907,965 23,907,965	3,901,956 11,760,024 2,094,401	2,779.8	307.094 478,512 70.718	32.292	367.094	E. 4.	12,000	46.727 24.929	6.0	76 39.504 1,500	322,914
Vermont Virginia Washington	1,867,573	3,765,387	3,166,369	1,867,452	3,410,217	141.0	267,062	37.959	211,141	4	986.08	59.917	4.7	121 34,263 3,825	5,335
West Virginia Wisconsin Wyoming	4, 474, 234 9, 724, 381 4, 501, 327	2,280,335	6.261.903	4,315,121 9,715,772 4,451,922	1.636.742	211.1 619.7 1.037.7	591,626 20,296 5,781	63.534	460,028 20,296	11.16		66,425	Proc. v	75,579 9,110 43,625	39,207
District of Columbia Hawaii	1,916,469	973,842	2,693,451	1,918,469	968.979	51.1	869.069		646.859	8.7		000*11		679	4,863 23,966
NEWS	995,000,000	200,000,000	522,136,677	387,368,764	179,213,648	34,890.2	19,011,209	4,082,745	13,123,351	9.624	862,349	2,946,839	138.0	1,686,142	1,716,162